

Virtual Testing of materials and structures undergoing corrosion and/or hydrogen embrittlement

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<https://www.imperial.ac.uk/mechanics-materials/>



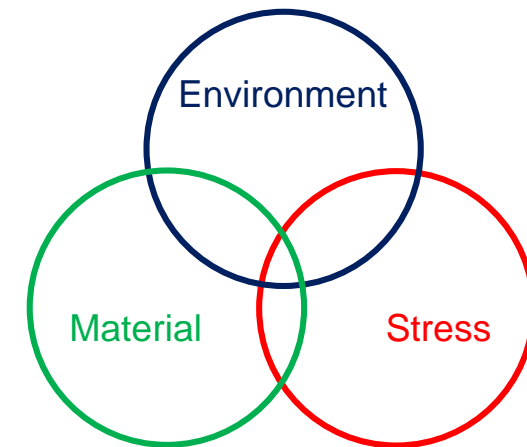
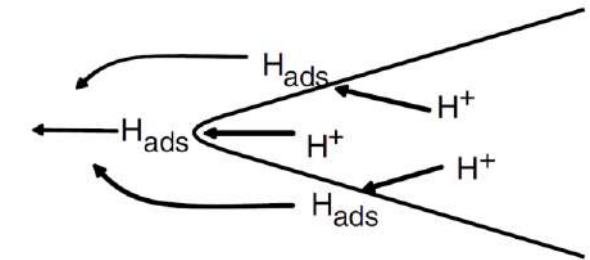
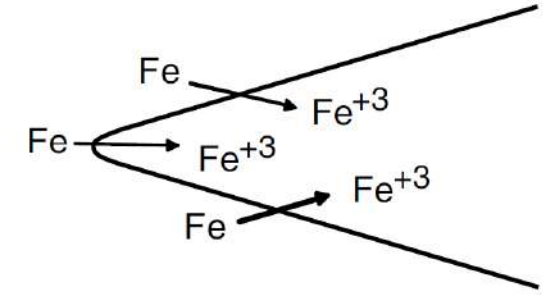
@MtnezPanedaE

With excellent contributions from:

T. Hageman (Imperial), P. Kristensen (DTU), A. Golahmar (DTU), C. Niordson (DTU), C. Cui (Imperial), S. Kovacevic (Imperial), M. Makuch (Imperial), M. Wenman (Imperial) and many others.

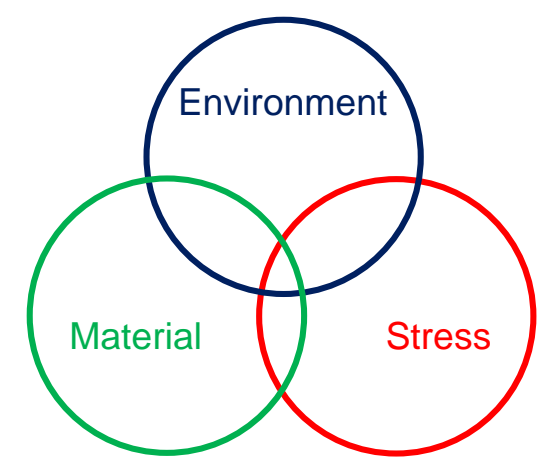
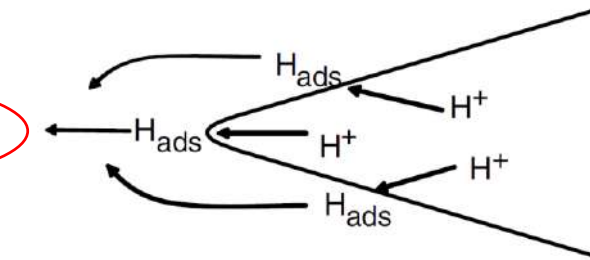
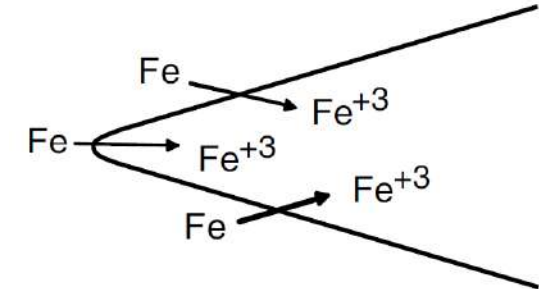
Environmentally
assisted cracking

- ☐ Stress Corrosion Cracking (SCC)
- ☐ Anodic-dissolution cracking
- ☐ Hydrogen embrittlement
- ☐ Hydrogen embrittlement
- ☐ Liquid Metal Embrittlement
- ☐ Oxidation fatigue, *etc.*

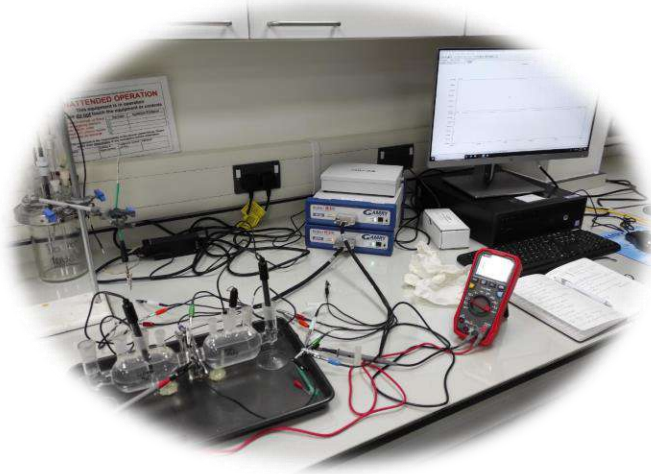


Environmentally
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- ☐ Stress Corrosion Cracking (SCC)
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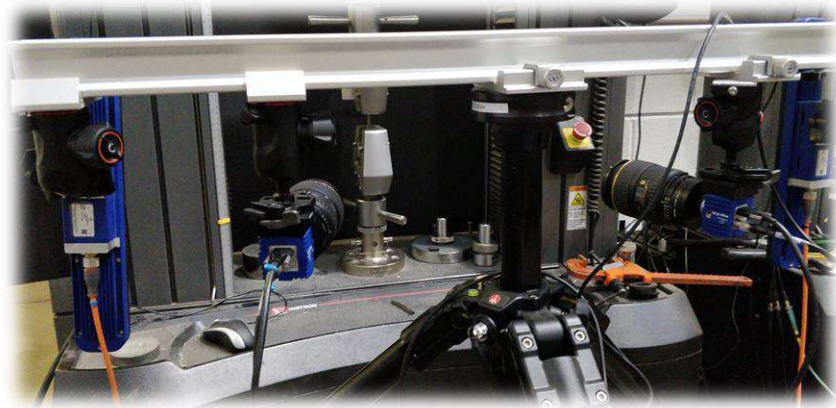
Permeation



E-chem charging



Desorption

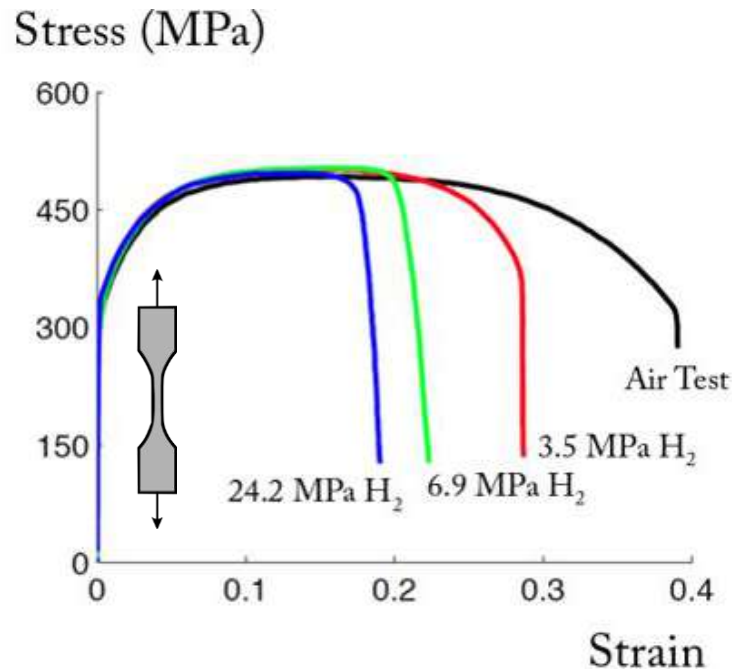


W. H. Johnson. Proceedings of the Royal Society of London Vol. 23, 168-179 (1875)

II. “On some remarkable Changes produced in Iron and Steel by the Action of Hydrogen and Acids.” By WILLIAM H. JOHNSON, B.Sc. Communicated by Prof. Sir WILLIAM THOMSON, LL.D., F.R.S. Received December 7, 1874.

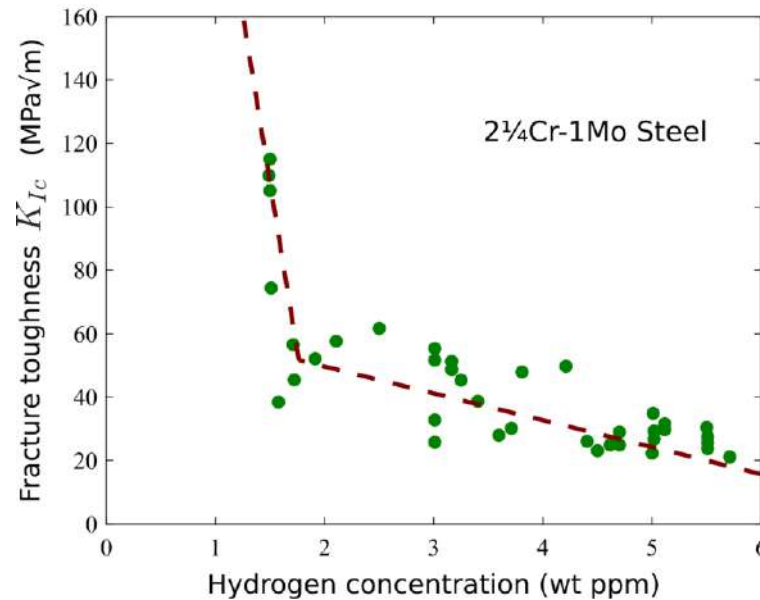
Some three years ago my attention was called to a remarkable change in some of the physical properties of iron caused by its temporary immersion in hydrochloric and sulphuric acids. This change is at once made evident to any one by the extraordinary decrease in toughness and breaking-strain of the iron so treated, and is all the more remarkable as it is

Ductility



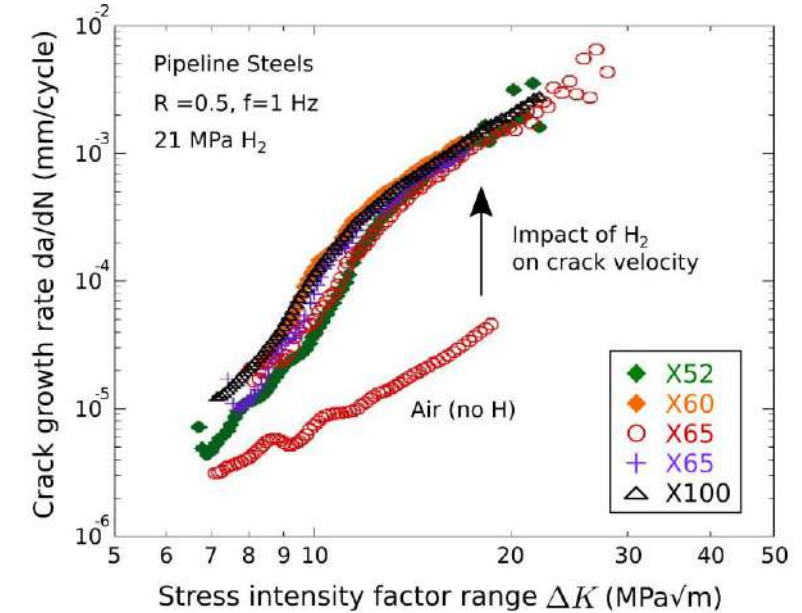
ASME SA106 Steel [Adapted from: Xu and Rana. 2008 *Int. Hydrogen Conference* (2009), Anand et al. *JMPS* (2019)]

Toughness



2 $\frac{1}{4}$ Cr-1Mo Steel [Adapted from: Hosseini et al. 2016 *Int. Hydrogen Conference* (2017)]

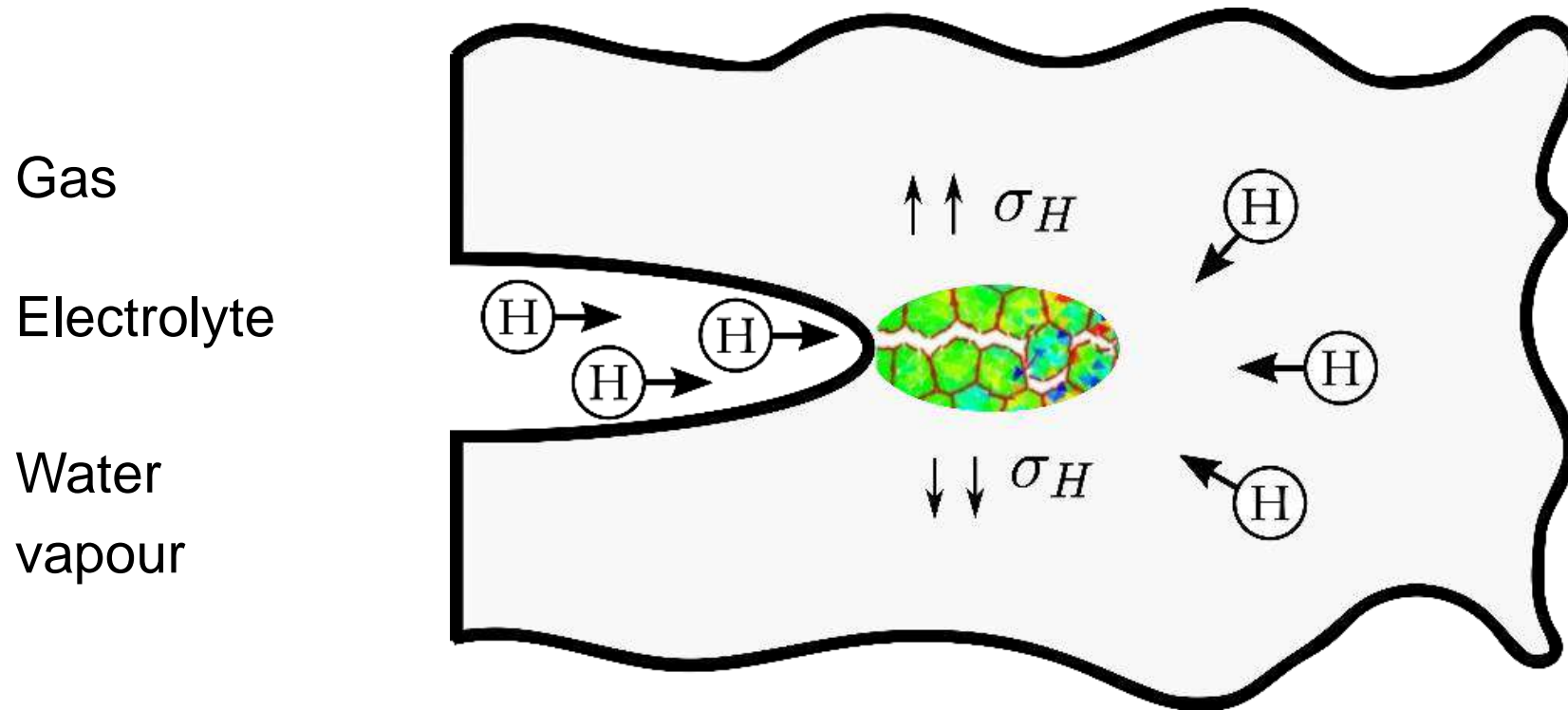
Fatigue crack growth



Pipeline steels [Adapted from: San Marchi & Ronevich, 2022 Symposium on Hydrogen- Materials Interactions]

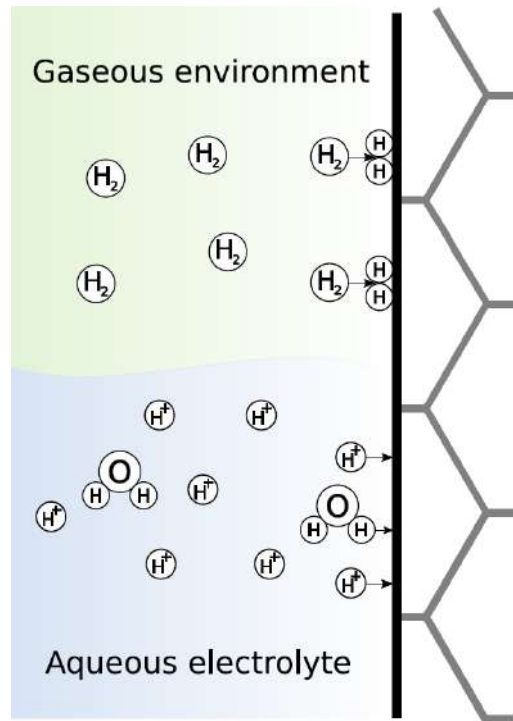
Hydrogen embrittlement: a complex phenomenon

Complex micromechanical and chemical problem, with hydrogen having an impact at multiple scales! [mechanics – chemistry – materials science]

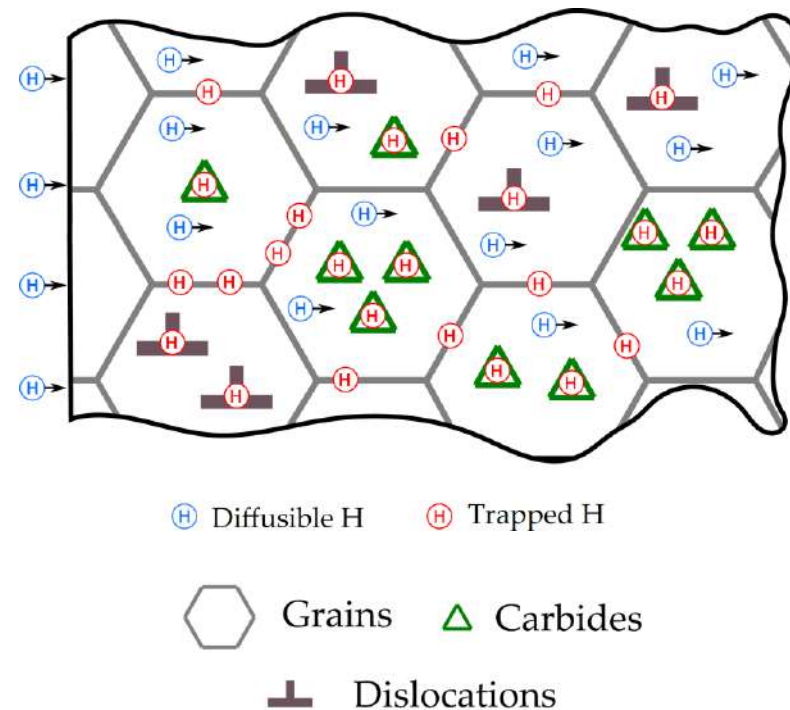


Hydrogen embrittlement stages

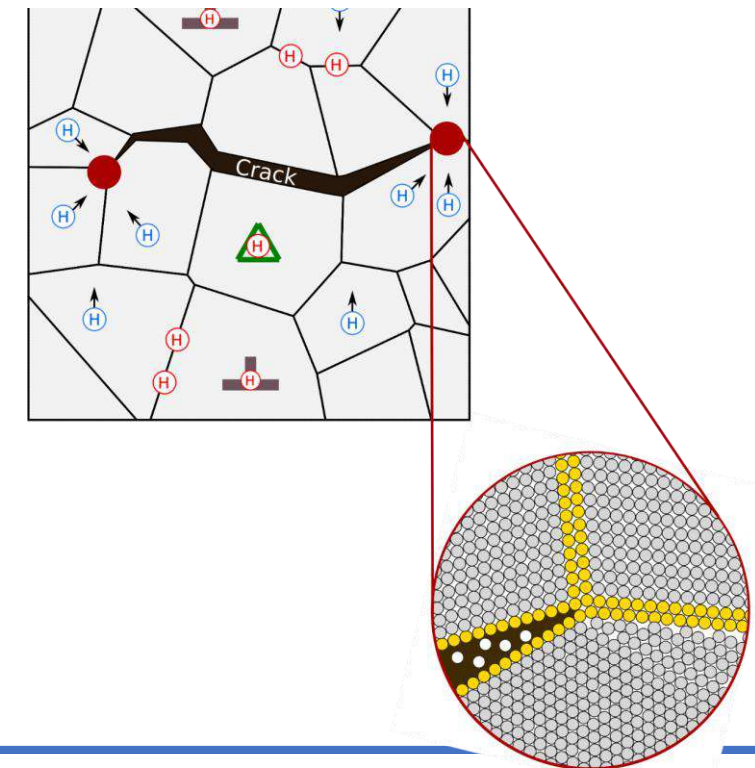
Stage I: H uptake



Stage II: H transport

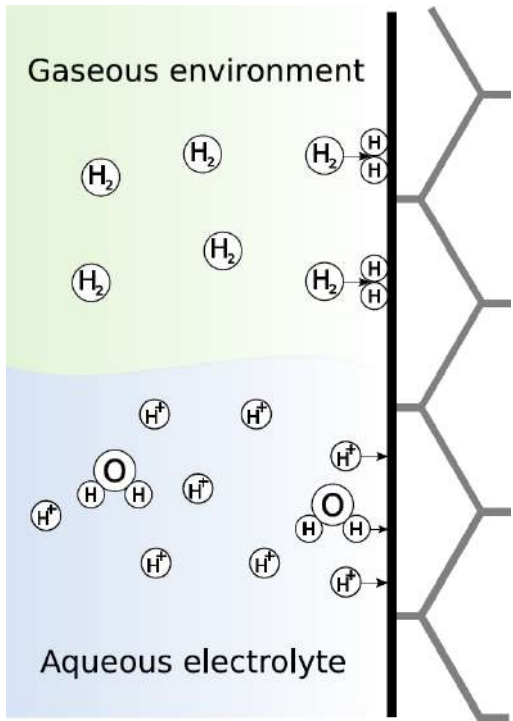


Stage III: H embrittlement

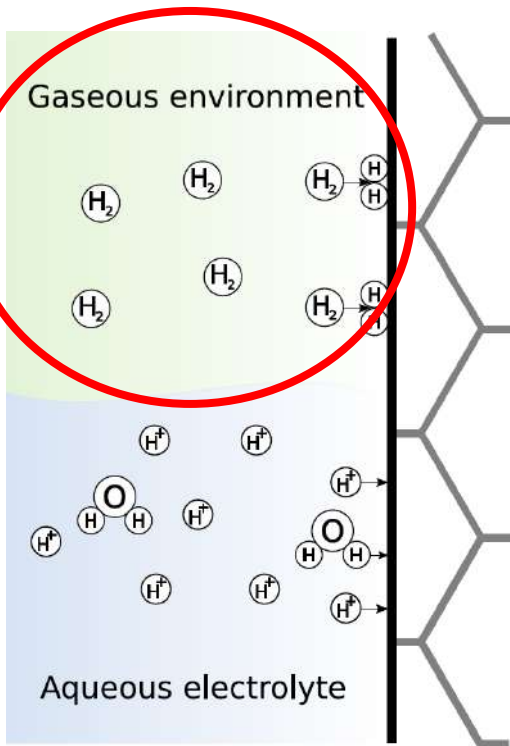


Stage I: H uptake

Stage I: H uptake



Stage I: H uptake



Gaseous environment (steady state)

$$\frac{1}{2}\mu_{H_2} = \mu_H \quad \text{with} \quad \mu_{H_2} = \mu_{H_2}^0 + RT \ln \left(\frac{f_{H_2}}{p^0} \right)$$

Hence: $\mu_H = RT \ln \left(\sqrt{\frac{f_{H_2}}{p^0}} \right)$ and recalling $\mu_L = \mu_L^0 + RT \ln \frac{\theta_L}{1 - \theta_L} - \bar{V}_H \sigma_H$

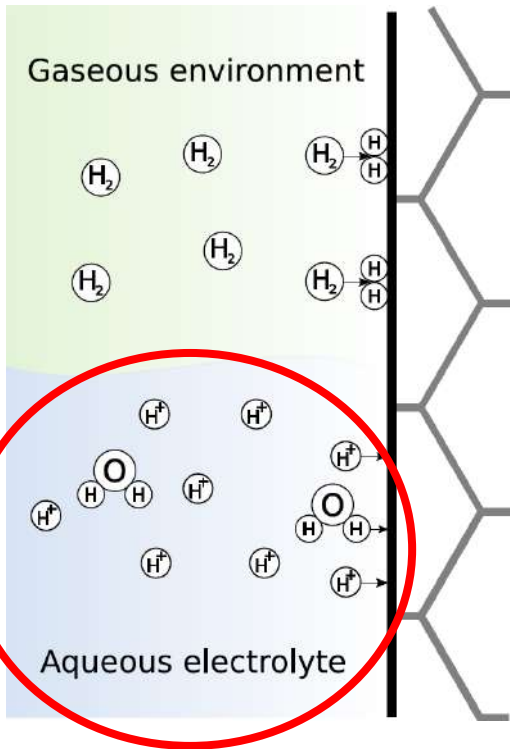
$$C_L = \frac{N_L}{\sqrt{p^0}} \exp \left(-\frac{\mu_L^0}{RT} \right) \exp \left(\frac{\bar{V}_H \sigma_H}{RT} \right) \sqrt{f_{H_2}}$$

$$C_L = K \sqrt{f_{H_2}} = \exp \left(\frac{\bar{V}_H \sigma_H}{RT} \right) K_{\sigma=0} \sqrt{f_{H_2}} \quad (\text{Sievert's law})$$

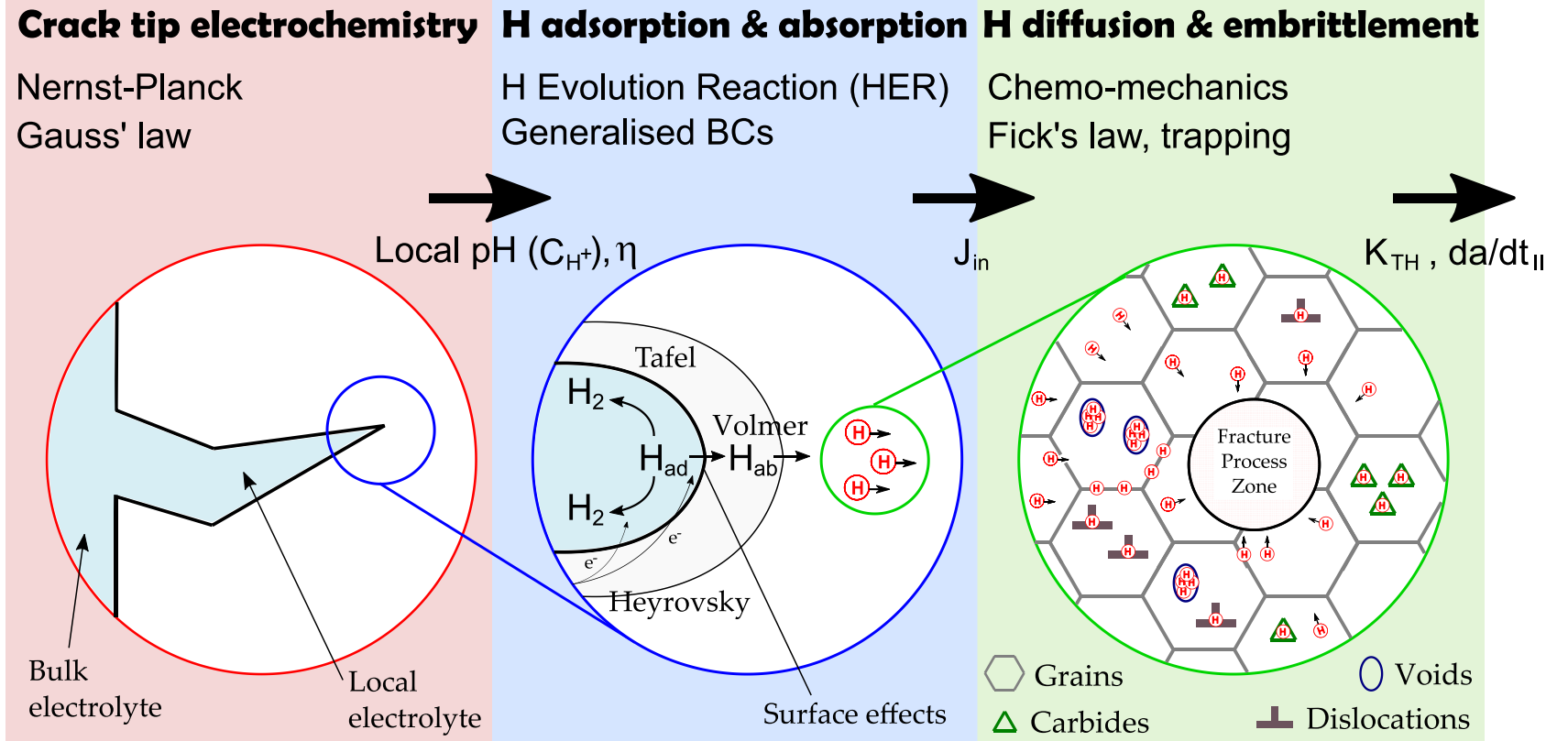
Díaz et al. *Int. J. Mech. Sci.* (2016)

Martínez-Pañeda et al. *Int. J. Hydrogen Energy* (2016)

Stage I: H uptake

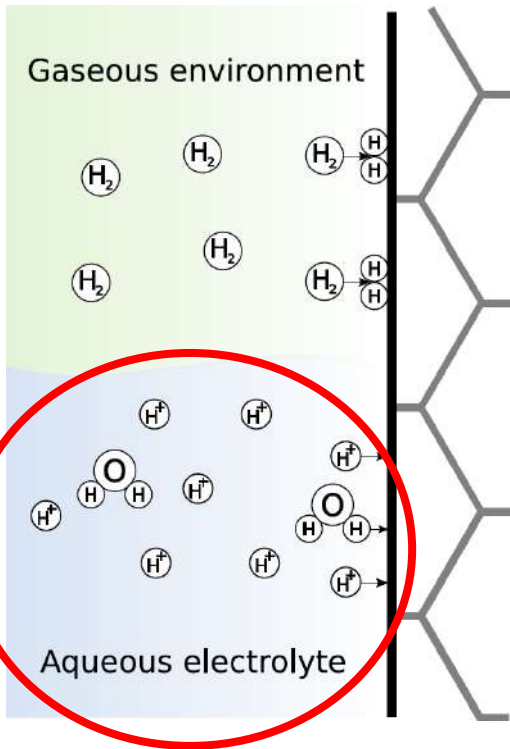


Aqueous electrolyte



Martínez-Pañeda. *RILEM Technical Letters* (2021)

Stage I: H uptake



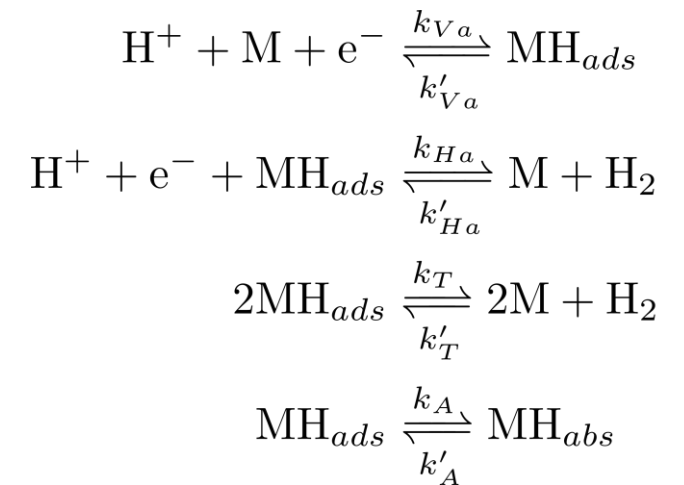
Aqueous electrolyte – a complete electro-chemo-mechanics model

Electrolyte domain

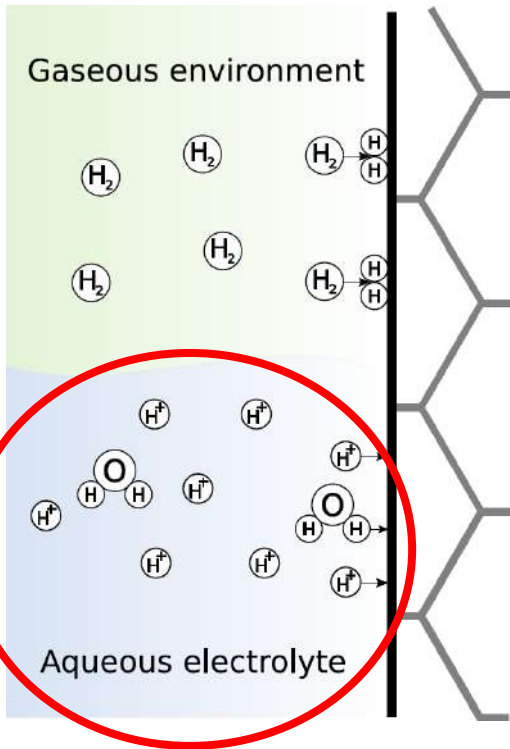
$$\text{Nernst-Planck: } \underbrace{\dot{C}_\pi + (\mathbf{v} \cdot \nabla) C_\pi}_{\text{transport due to fluid flow}} + \underbrace{\nabla \cdot (-D_\pi \nabla C_\pi)}_{\text{diffusion}} + \underbrace{\frac{z_\pi F}{RT} \nabla \cdot (-D_\pi C_\pi \nabla \varphi)}_{\text{electric potential driven migration}} + \underbrace{R_\pi}_{\text{volume reactions}} = 0$$

$$\text{Electro-neutrality: } \sum_{\pi} z_\pi C_\pi = 0$$

Surface domain



Stage I: H uptake



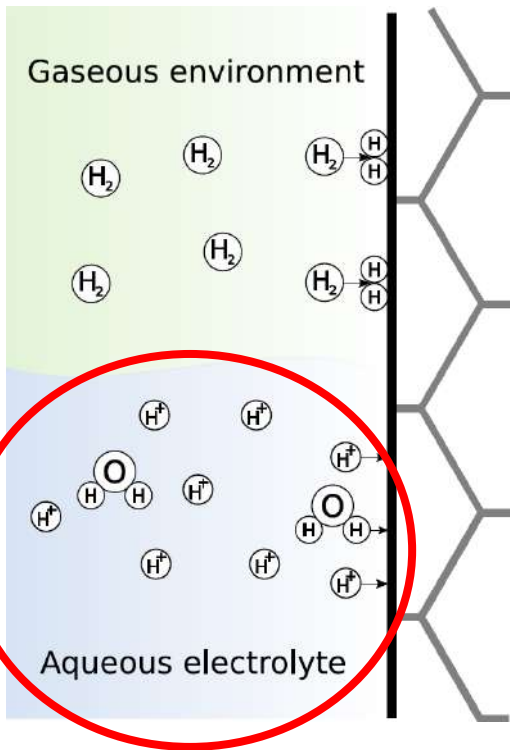
Aqueous electrolyte – a complete electro-chemo-mechanics model

Reaction rates:

	Forward	Backward
Volmer(acid) :	$\nu_{Va} = k_{Va} C_{H^+} (1 - \theta_{ads}) \exp\left(-\alpha_{Va} \frac{\eta F}{RT}\right)$	$\nu'_{Va} = k'_{Va} \theta_{ads} \exp\left((1 - \alpha_{Va}) \frac{\eta F}{RT}\right)$
Heyrovsky(acid) :	$\nu_{Ha} = k_{Ha} C_{H^+} \theta_{ads} \exp\left(-\alpha_{Ha} \frac{\eta F}{RT}\right)$	$\nu'_{Ha} = k'_{Ha} (1 - \theta_{ads}) p_{H_2} \exp\left((1 - \alpha_{Ha}) \frac{\eta F}{RT}\right)$
Tafel :	$\nu_T = k_T \theta_{ads}^2$	$\nu'_T = k'_T (1 - \theta_{ads})^2 p_{H_2}$
Absorption :	$\nu_A = k_A (N_L - C_L) \theta_{ads}$	$\nu'_A = k'_A C_L (1 - \theta_{ads})$
Volmer(base) :	$\nu_{Vb} = k_{Vb} (1 - \theta_{ads}) \exp\left(-\alpha_{Vb} \frac{\eta F}{RT}\right)$	$\nu'_{Vb} = k'_{Vb} C_{OH^-} \theta_{ads} \exp\left((1 - \alpha_{Vb}) \frac{\eta F}{RT}\right)$
Heyrovsky(base) :	$\nu_{Hb} = k_{Hb} \theta_{ads} \exp\left(-\alpha_{Hb} \frac{\eta F}{RT}\right)$	$\nu'_{Hb} = k'_{Hb} (1 - \theta_{ads}) p_{H_2} C_{OH^-} \exp\left((1 - \alpha_{Hb}) \frac{\eta F}{RT}\right)$

Stage I: H uptake, aqueous electrolyte

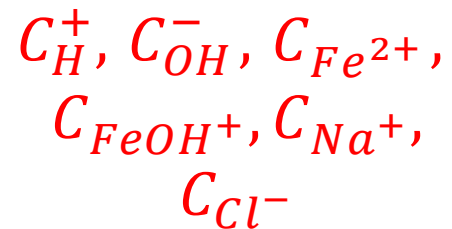
Stage I: H uptake



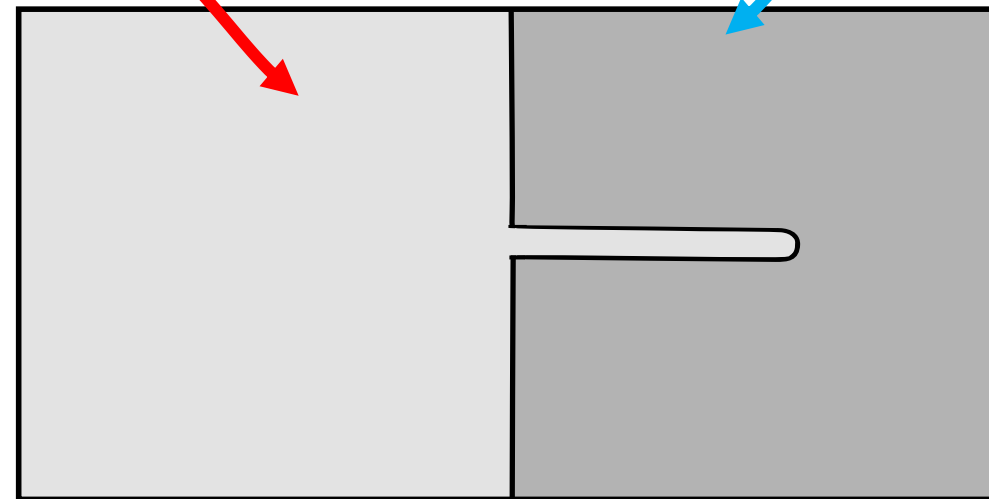
Aqueous electrolyte – a complete electro-chemo-mechanics model

Electrolyte:

Ion species



Electric potential

 φ


Metal:

Displacement

 u

Lattice H concentration

 C_L

Metal surface:

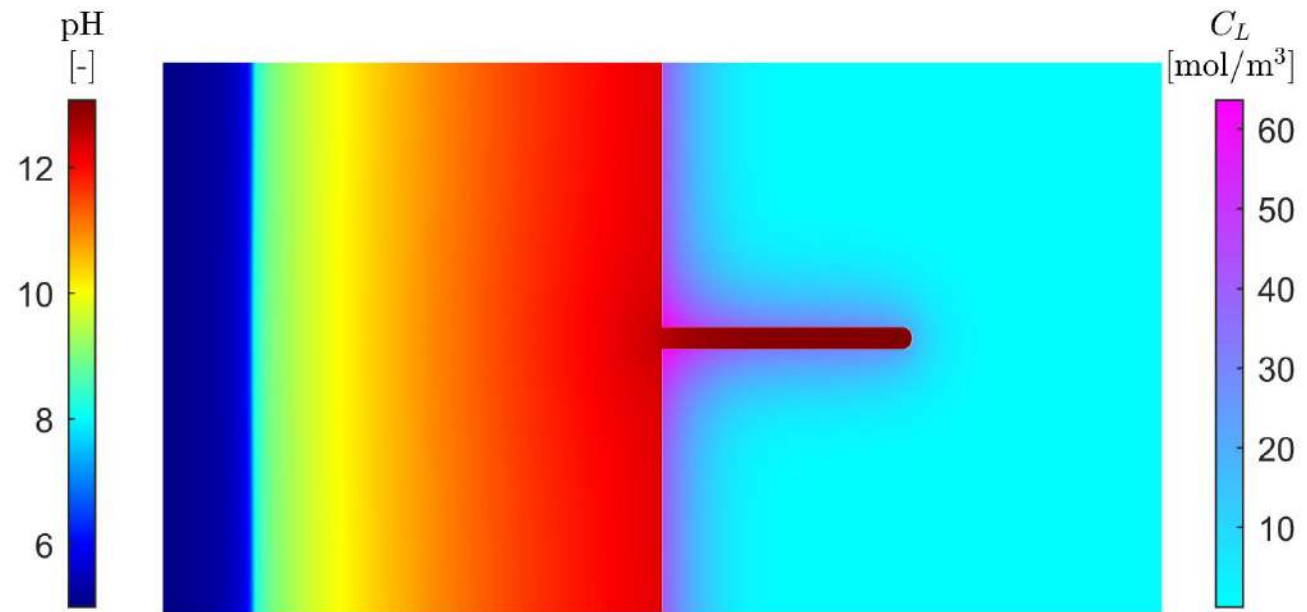
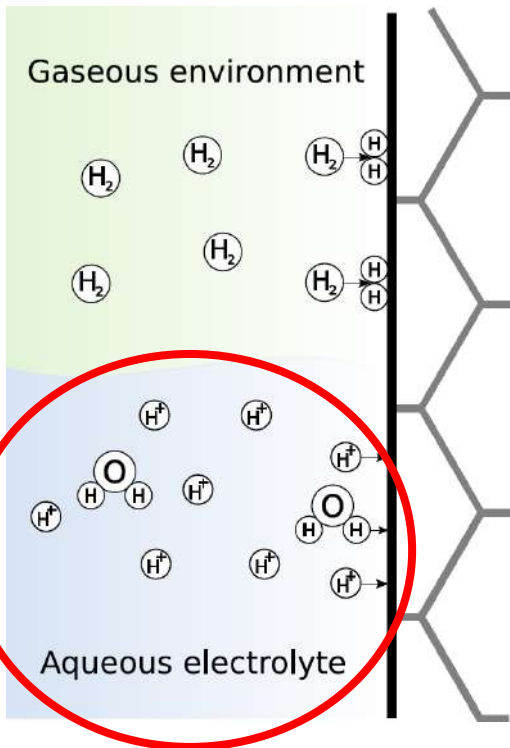
Surface coverage θ_{ads}

Hageman & Martínez-Pañeda. *Corros. Sci.* (2022)

Stage I: H uptake, aqueous electrolyte

Stage I: H uptake

Aqueous electrolyte – a complete electro-chemo-mechanics model

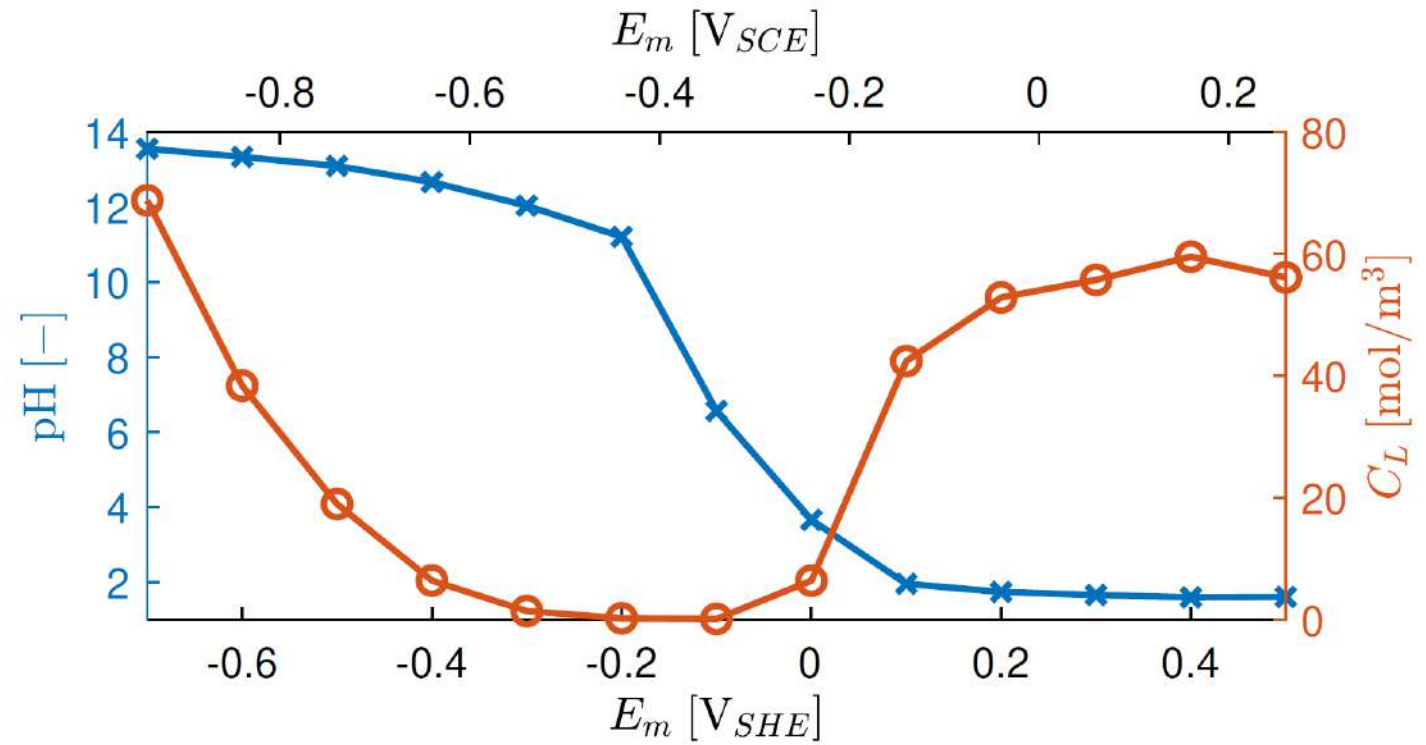
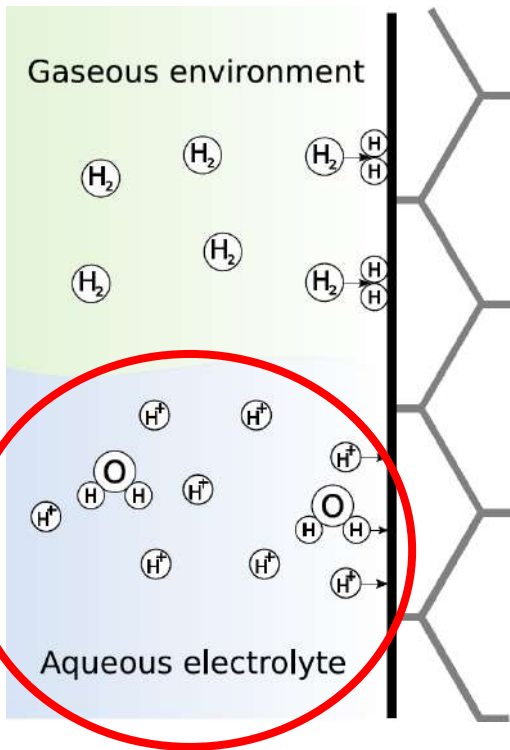


$$E_M = -0.5 V_{SHE}$$

Stage I: H uptake

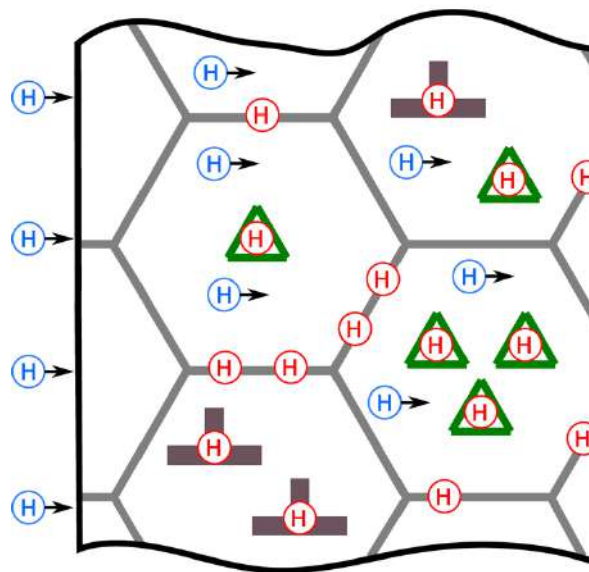
Aqueous electrolyte – a complete electro-chemo-mechanics model

Crack tip estimates:



Stage II: H diffusion and trapping

Stage II: H transport

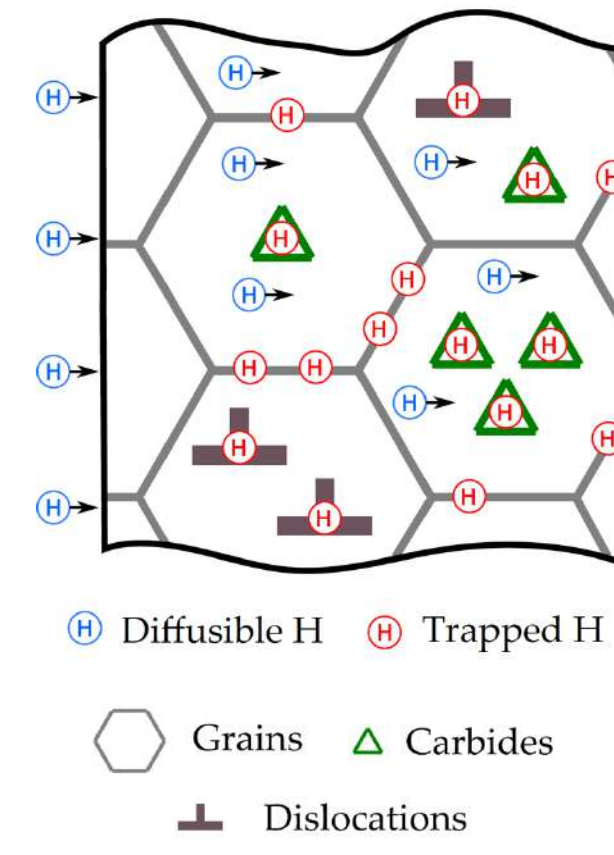


⊕ Diffusible H ⊗ Trapped H

⬡ Grains ▲ Carbides

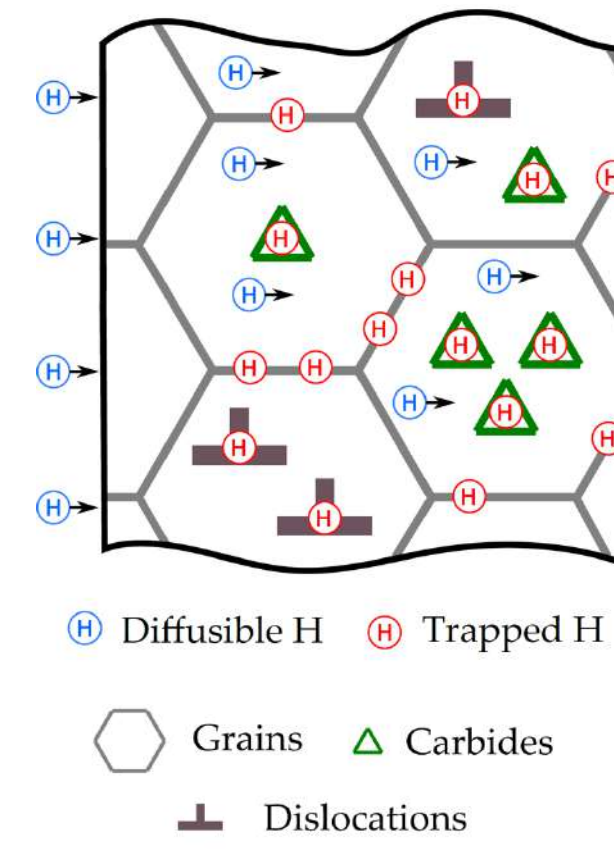
⊥ Dislocations

Stage II: H transport



$$\frac{\partial C}{\partial t} - D\nabla^2 C + \nabla \cdot \left(\frac{DC}{RT} \bar{V}_H \nabla \sigma_H \right) = 0$$

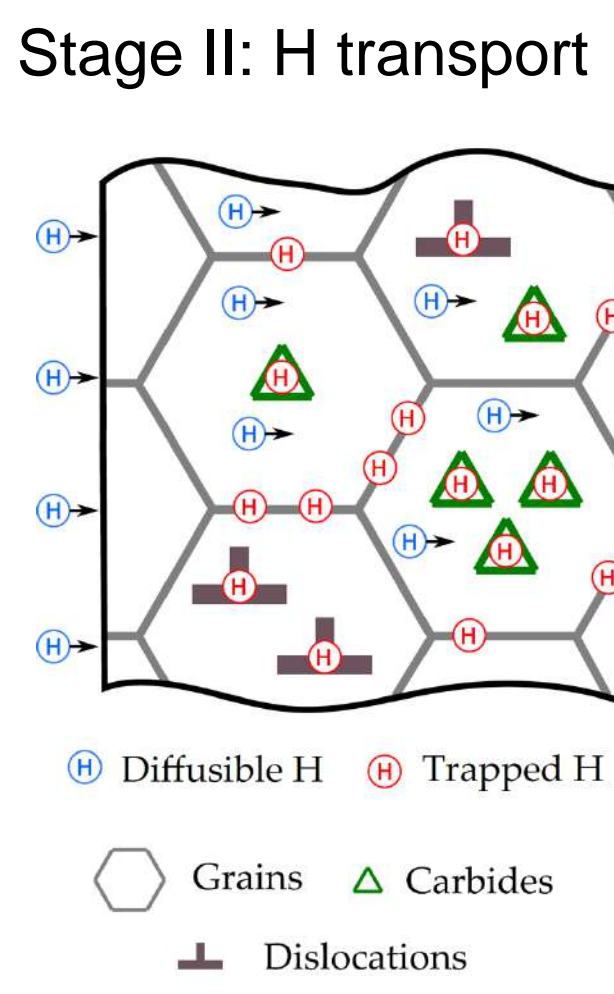
Stage II: H transport



$$\frac{\partial C}{\partial t} - D\nabla^2 C + \nabla \cdot \left(\frac{DC}{RT} \bar{V}_H \nabla \sigma_H \right) = 0$$

At steady-state: $C_L = C_0 \exp \left(\frac{\bar{V}_H \sigma_H}{RT} \right)$

Stage II: H transport



Oriani multi-trap

$$C_L = N_L \theta_L \quad , \quad C_T = N_T \theta_T \quad , \quad D_e = D \frac{C_L}{C_L + \sum_i C_T^{(i)} (1 - \theta_T^{(i)})}$$

$$\frac{D_L}{D_e} \frac{\partial C_L}{\partial t} = D_L \nabla^2 C_L + \nabla \cdot \left(\frac{D_L C_L}{RT} \bar{V}_H \nabla \sigma_H \right)$$

Isfandbod & Martínez-Pañeda. *Int. J. Plast.* (2021)

Fernández-Sousa, Betegón, Martínez-Pañeda. *Acta Mat.* (2020)

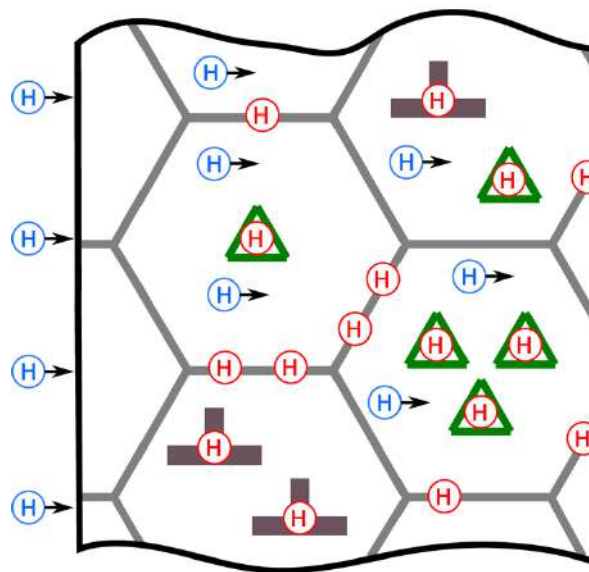
McNabb-Foster

$$\frac{\partial C_L}{\partial t} + \frac{\partial C_T}{\partial t} = D_L \nabla^2 C_L + \nabla \cdot \left(\frac{D_L C_L}{RT} \bar{V}_H \nabla \sigma_H \right)$$

$$\frac{\partial C_T}{\partial t} = N_T [k_r C_L (1 - \theta_T) - p_r \theta_T]$$

Martínez-Pañeda, Díaz, Wright, Turnbull. *Corros. Sci.* (2020)

Stage II: H transport



⊕ Diffusible H ⊕ Trapped H

⬡ Grains ▲ Carbides

⊥ Dislocations

Oriani multi-trap

$$C_L = N_L \theta_L, \quad C_T = N_T \theta_T, \quad D_e = D \frac{C_L}{C_L + \sum_i C_T^{(i)} (1 - \theta_T^{(i)})}$$

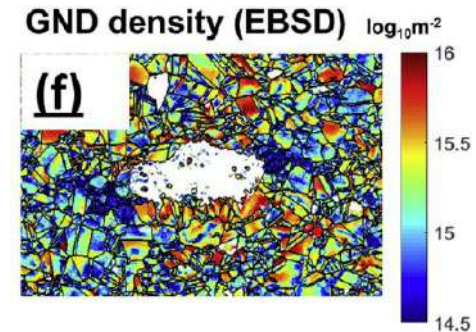
$$\frac{D_L}{D_e} \frac{\partial C_L}{\partial t} = D_L \nabla^2 C_L + \nabla \cdot \left(\frac{D_L C_L}{RT} \bar{V}_H \nabla \sigma_H \right)$$

➤ Dislocation trap density account for SSDs and GNDs:

$$N_T^{(d)} = \frac{\sqrt{2}\rho}{a} \quad \text{with} \quad \rho = \rho_{SSD} + \rho_{GND}$$

Taylor (1938):

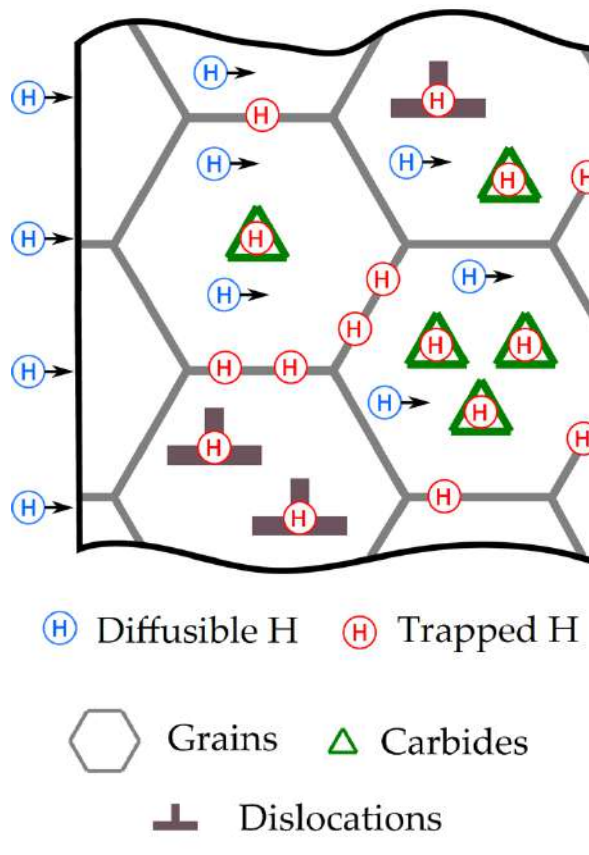
$$\rho_{GND} = \bar{r} \frac{\eta^p}{b} \quad \rho_{SSD} = \left(\frac{\sigma_{ref} f(\epsilon^p)}{0.5 M \mu b} \right)^2$$



J. Jiang et al., Acta Mater., 2016

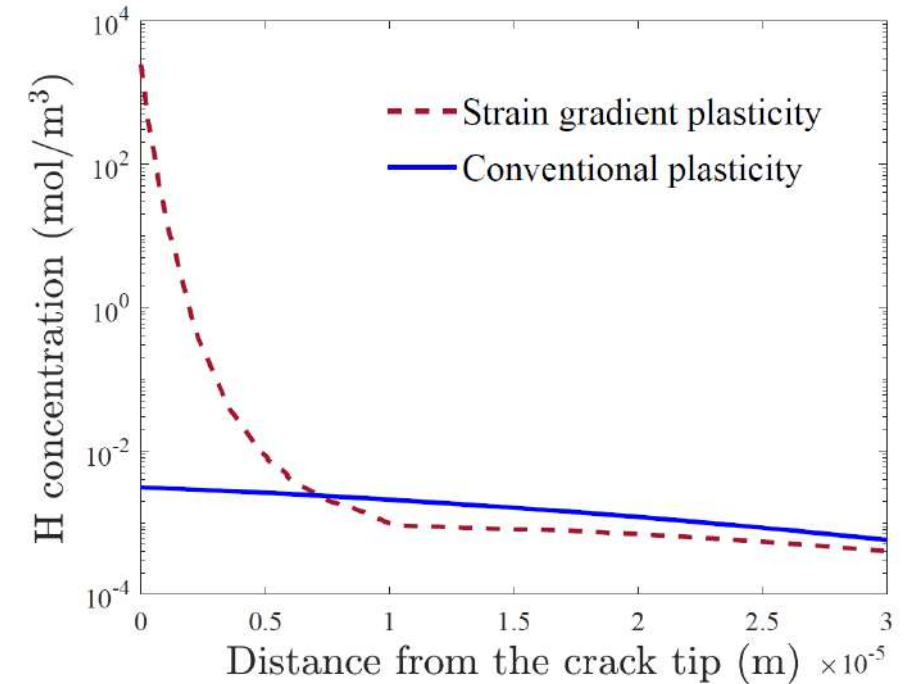
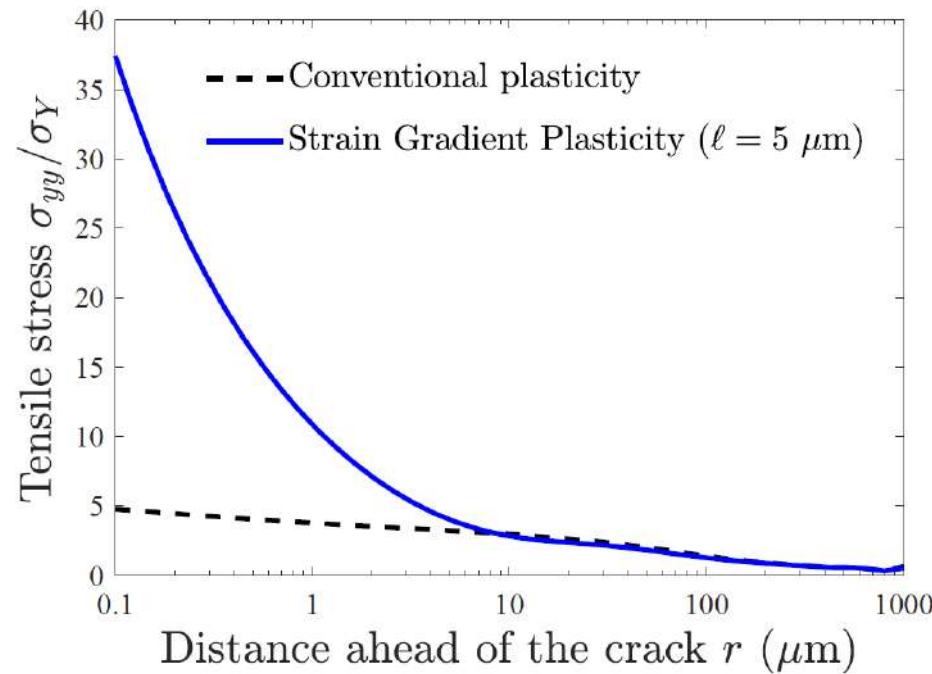
Martínez-Pañeda, Niordson, Gangloff. Acta Mater. (2016)

Stage II: H transport



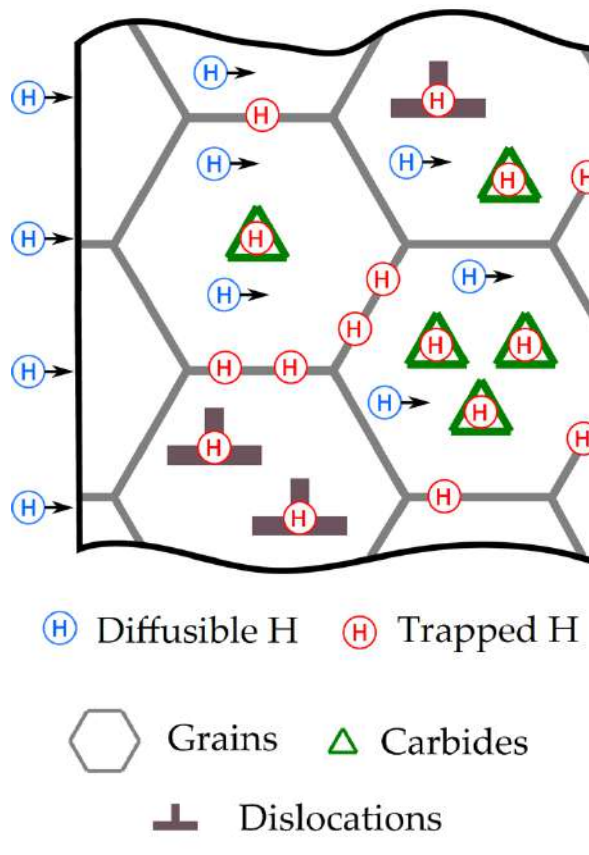
The dual role of GNDs: enhancing trapping and elevating σ_H and C_L

$$\sigma_f = 0.5M\mu b\sqrt{\rho} = 0.5M\mu b\sqrt{\rho_{SSD} + \rho_{GND}}$$

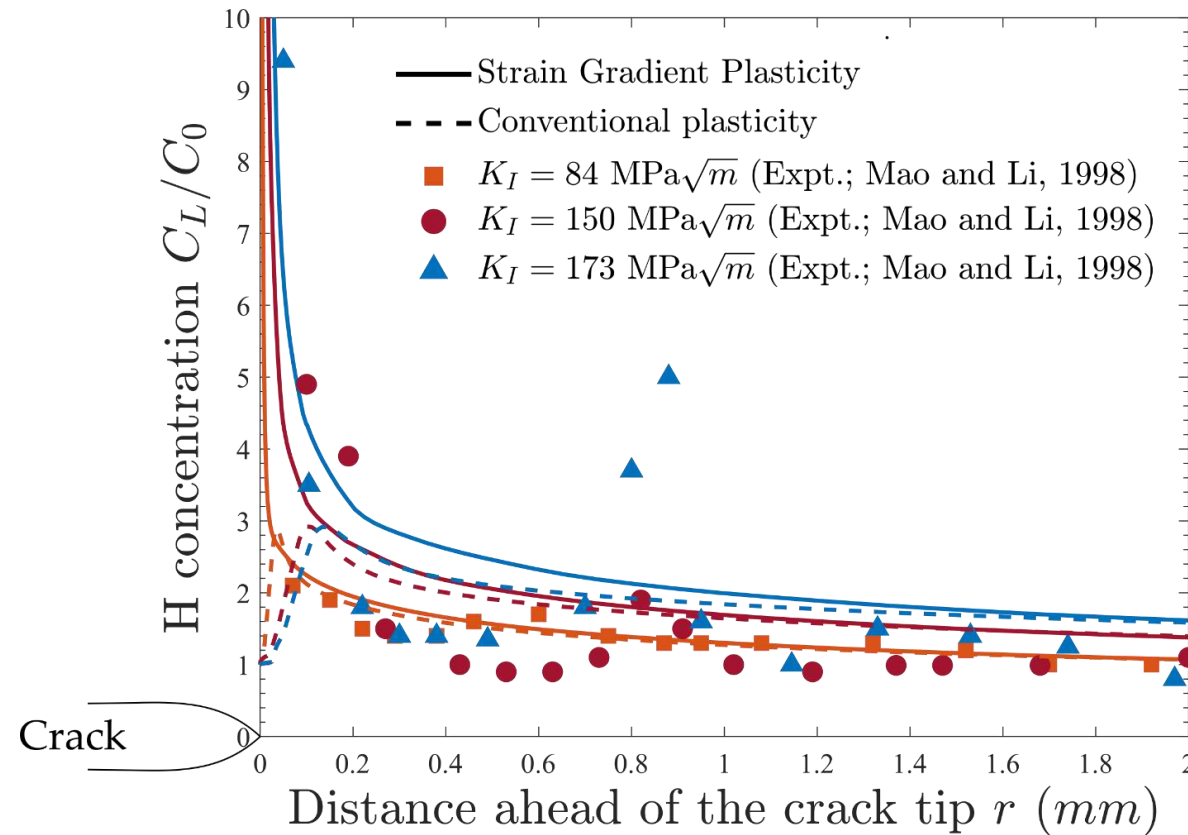


Martínez-Pañeda et al. *Int. J. Hydrogen Energy* (2016)

Stage II: H transport

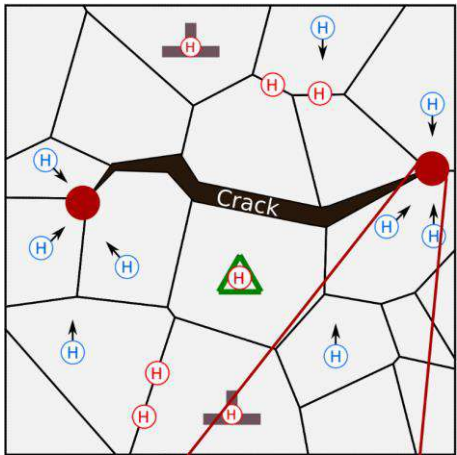


The dual role of GNDs: enhancing trapping and elevating σ_H and C_L

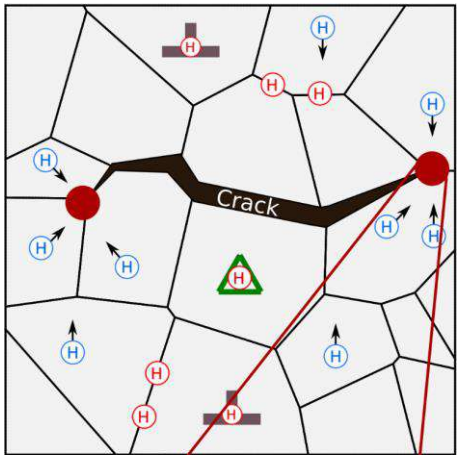


Martínez-Pañeda et al. *Int. J. Hydrogen Energy* (2016)

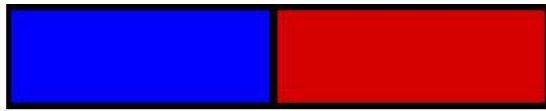
Stage III: Fracture



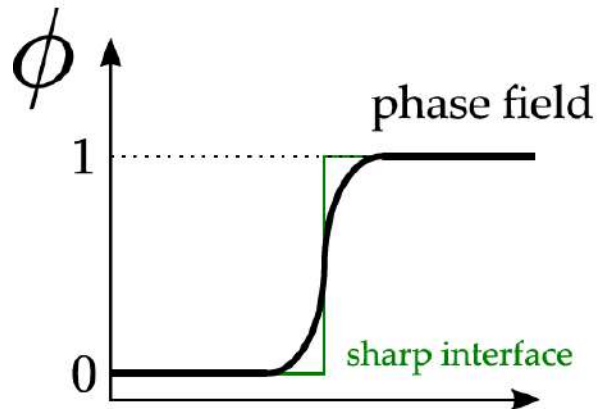
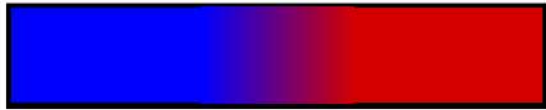
Stage III: Fracture



Phase field modelling

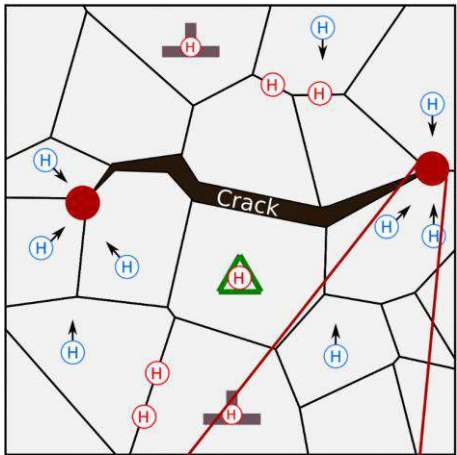


VS

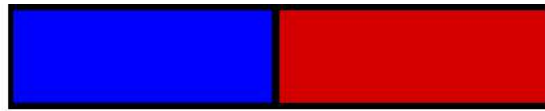


Stage III: Embrittlement

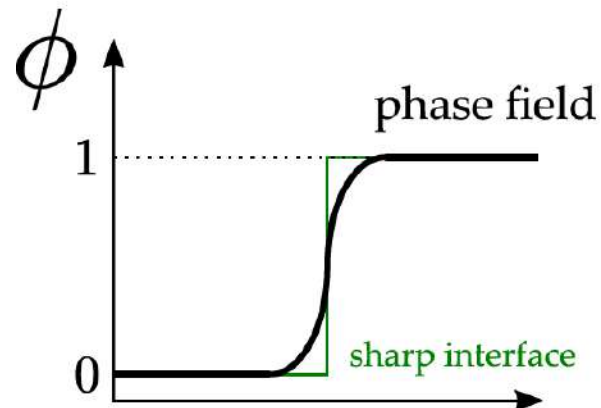
Stage III: Fracture



Phase field modelling



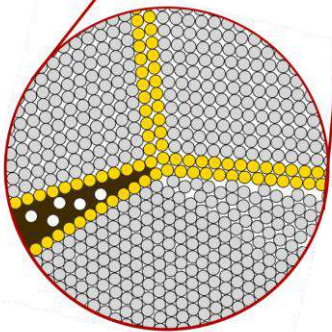
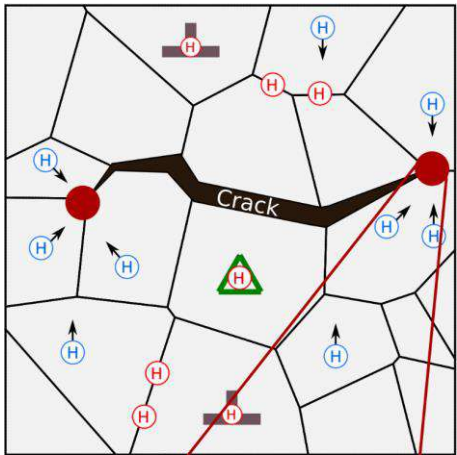
VS



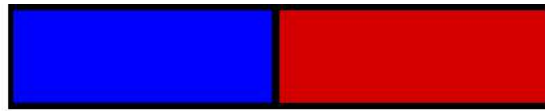
- The interface equation is defined in the entire domain, no special treatment is needed
- Topological changes such as divisions or merging of interfaces can be easily simulated
- The interface equation can be easily combined with equations describing various physical phenomena

Stage III: Embrittlement

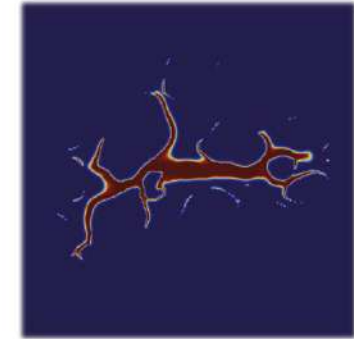
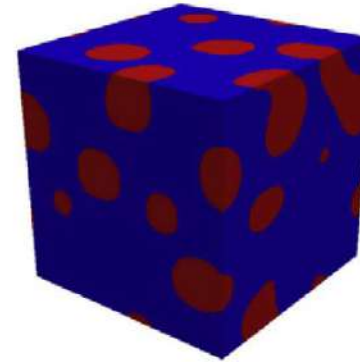
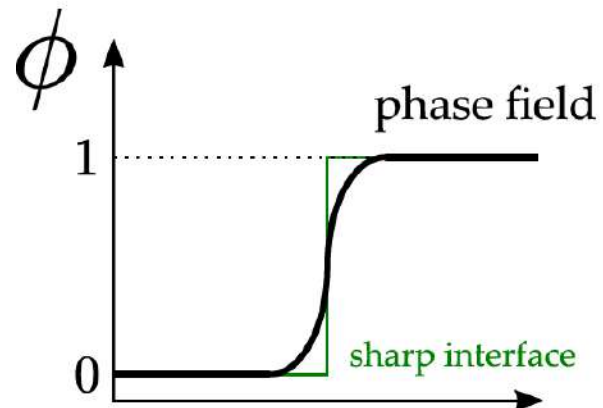
Stage III: Fracture



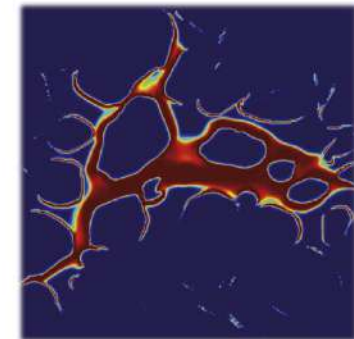
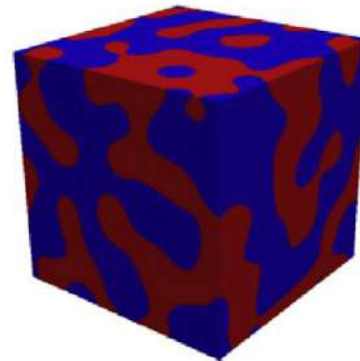
Phase field modelling



VS



t_0

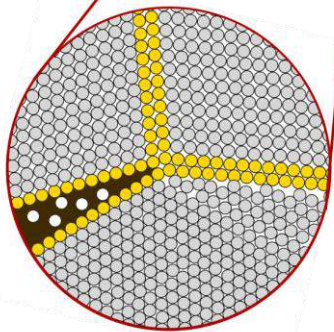
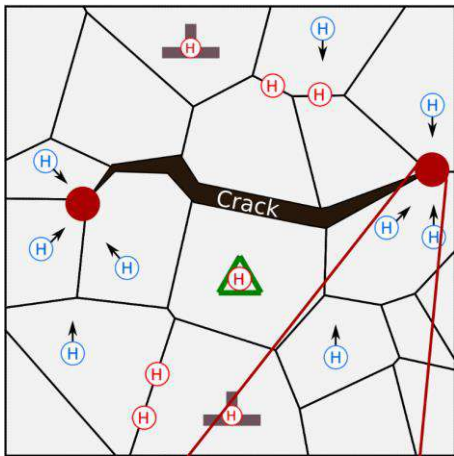


t_1

Microstructural evolution

Fracture mechanics

Stage III: Fracture



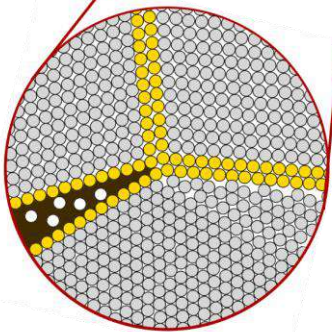
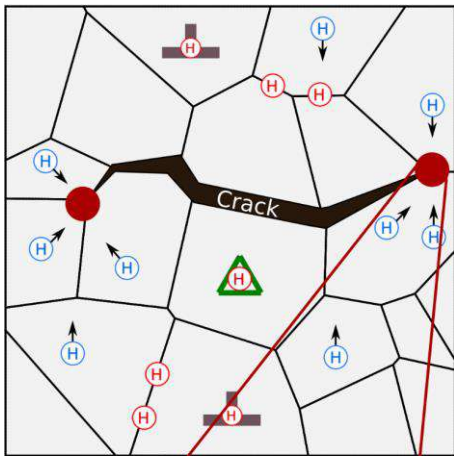
Phase field fracture

- Griffith's energy balance (Griffith, 1920)

$$\frac{d\Pi}{dA} = \frac{d\Psi(\epsilon)}{dA} + G_c = 0$$

A - crack area $\Psi = \int \psi dV$ - strain energy
 Π - total energy G_c - critical energy release rate

Stage III: Fracture



Phase field fracture

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$$\frac{d\Pi}{dA} = \frac{d\Psi(\epsilon)}{dA} + G_c = 0$$

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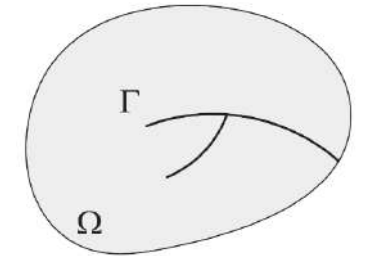
$$\Psi = \int \psi dV \text{ - strain energy}$$

Π - total energy

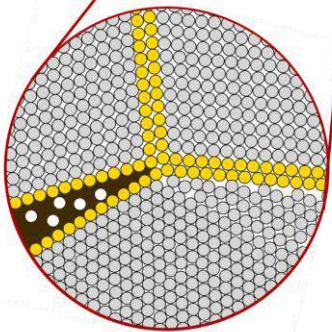
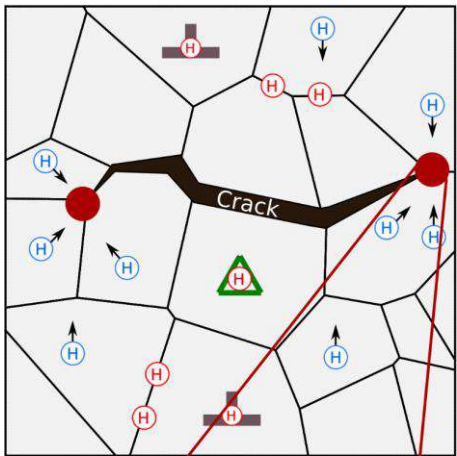
G_c - critical energy release rate

- Variational approach to fracture (Francfort and Marigo, 1998)

$$\Pi = \int_{\Omega} \psi(\epsilon) dV + \int_{\Gamma} G_c d\Gamma$$



Stage III: Fracture



Phase field fracture

- Griffith's energy balance (Griffith, 1920)

$$\frac{d\Pi}{dA} = \frac{d\Psi(\epsilon)}{dA} + G_c = 0$$

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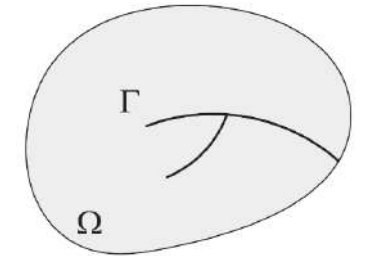
$$\Psi = \int \psi dV \text{ - strain energy}$$

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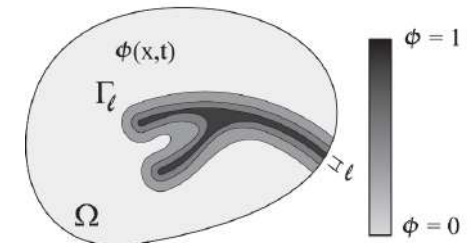
- Variational approach to fracture (Francfort and Marigo, 1998)

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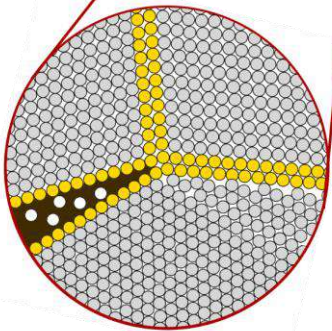
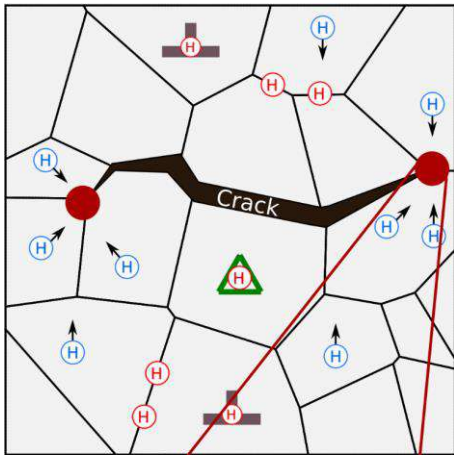


- Phase field fracture (Bourdin et al., 2008; Miehe et al., 2010)

$$\Pi_{\ell} = \int_{\Omega} (1 - \phi)^2 \psi_0(\epsilon) dV + \int_{\Omega} G_c \left(\frac{\phi^2}{2\ell} + \frac{\ell}{2} |\nabla\phi|^2 \right) dV$$



Stage III: Fracture

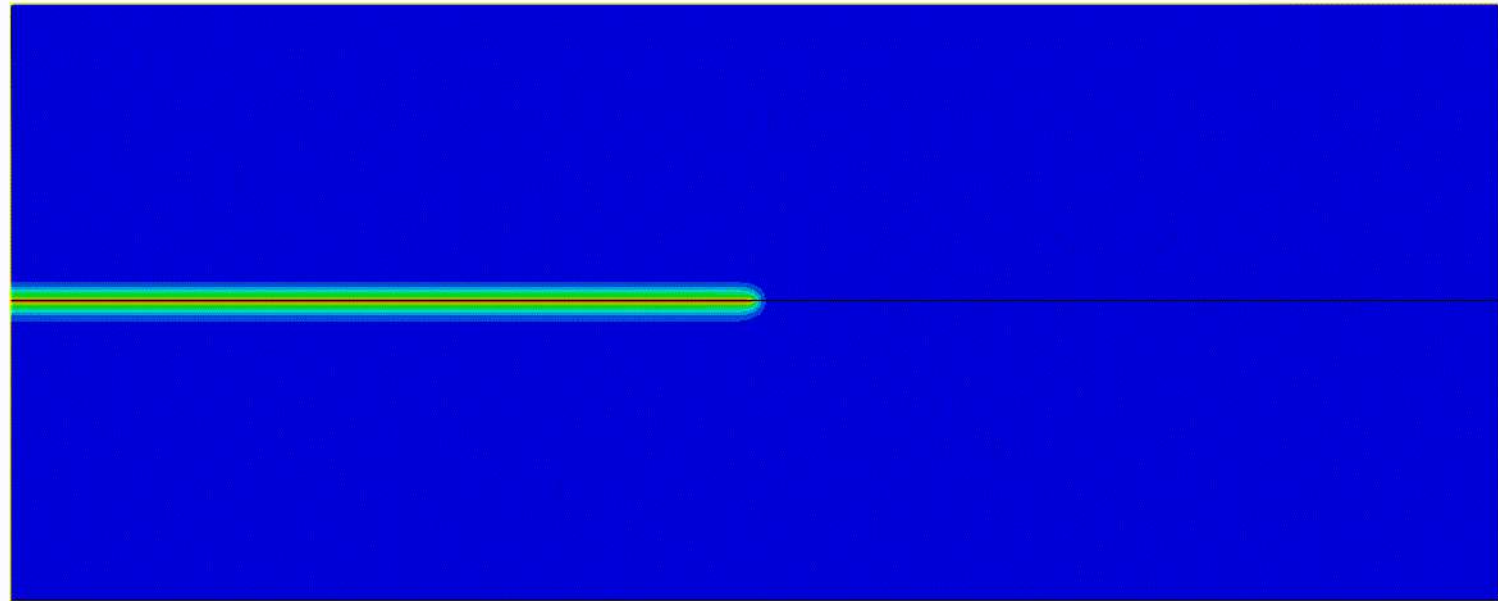


Phase field fracture

Balance equations:

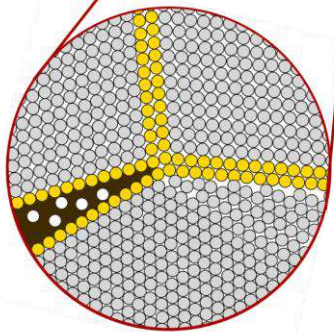
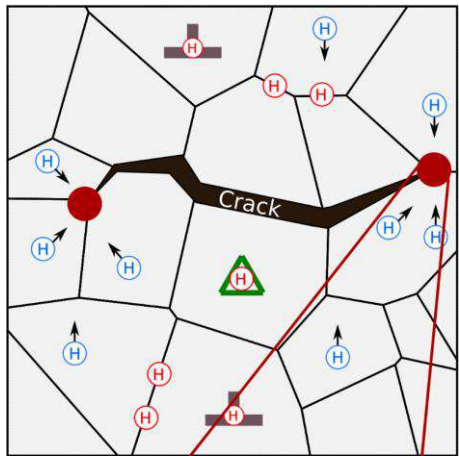
$$\nabla \cdot \left[(1 - \phi)^2 \boldsymbol{\sigma} \right] = \mathbf{0} \quad \text{in } \Omega \quad \text{red} - \text{cracked material}$$

$$G_c \left(\frac{\phi}{\ell} - \ell \nabla^2 \phi \right) - 2(1 - \phi) \psi_0(\boldsymbol{\varepsilon}) = 0 \quad \text{in } \Omega \quad \text{blue} - \text{intact material}$$

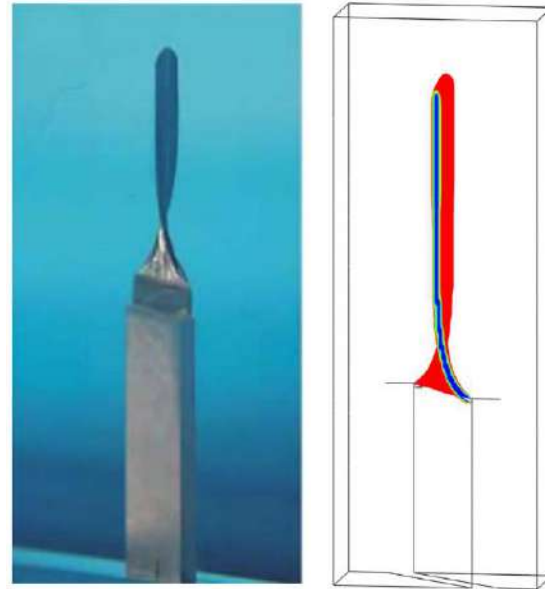


Kristensen, Niordson, Martínez-Pañeda. *Theor. Appl. Fract. Mech.* (2020)

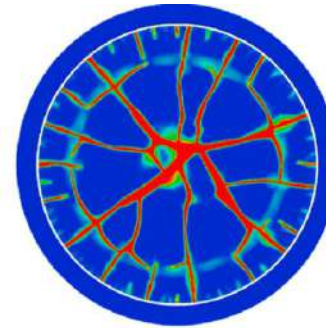
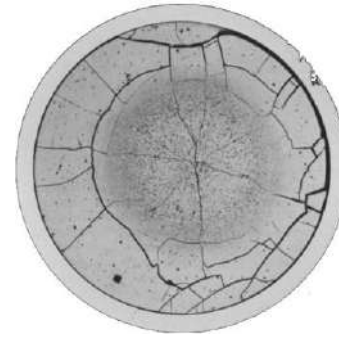
Stage III: Fracture



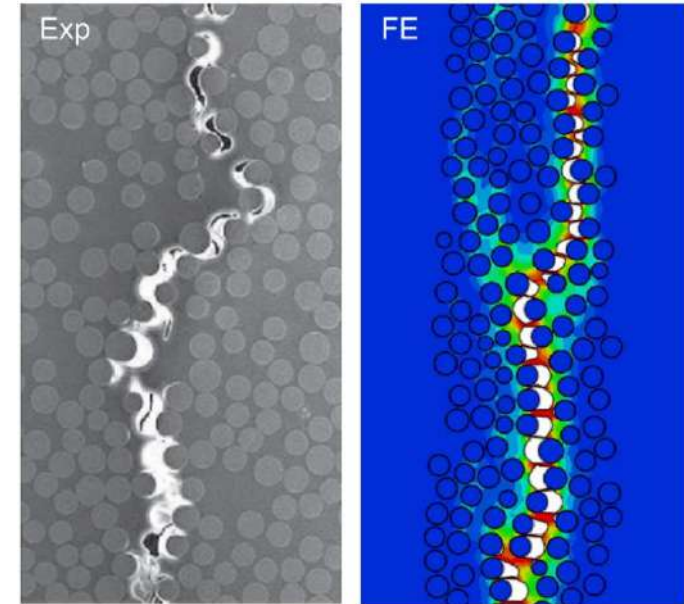
Phase field fracture



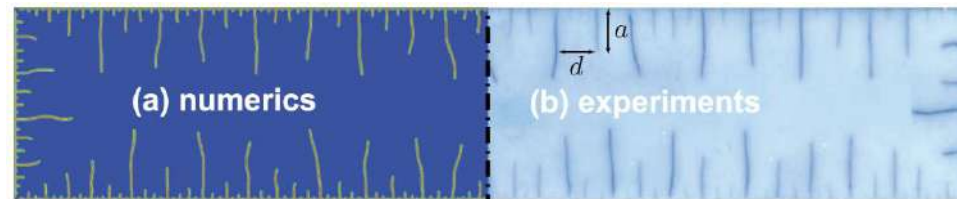
Wu et al., *CMAME* (2021)



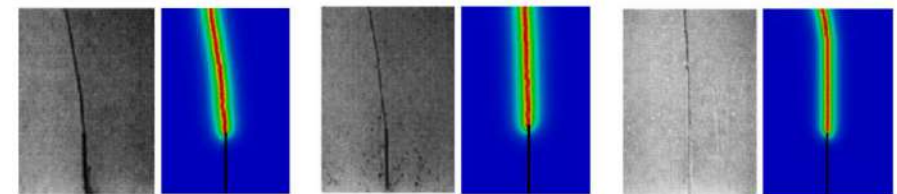
Li & Shirvan, *Ceram. Int.* (2021)



Tan & Martínez-Pañeda, *Compos. Sci. Technol.* (2021)

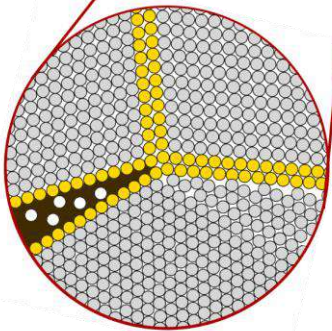
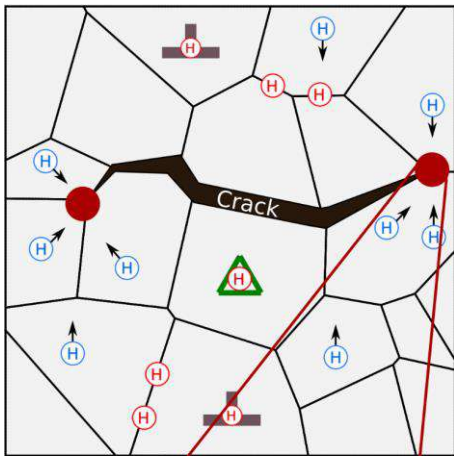


Bourdin et al., *Phys. Rev. Lett.* (2014)



Hirshikesh, Natarajan, Martínez-Pañeda. *Composites, Part B* (2019)

Stage III: Fracture



Phase field modelling of H embrittlement

Deformation of the solid:

$$\nabla \cdot \left[(1 - \phi)^2 \boldsymbol{\sigma} \right] = \mathbf{0}$$

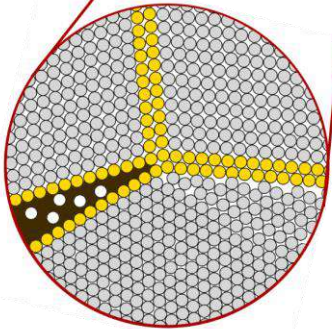
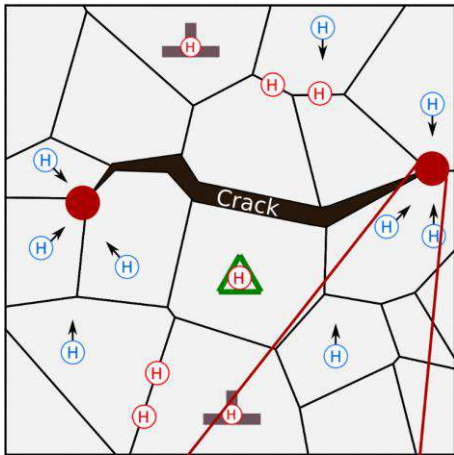
Hydrogen transport:

$$\frac{\partial C}{\partial t} - D \nabla^2 C + \nabla \cdot \left(\frac{DC}{RT} \bar{V}_H \nabla \sigma_H \right) = 0$$

Damage:

$$G_c \left(\frac{\phi}{\ell} - \ell \nabla^2 \phi \right) - 2(1 - \phi) \psi(\boldsymbol{\varepsilon}) = 0$$

Stage III: Fracture



Phase field modelling of H embrittlement

Deformation of the solid:

$$\nabla \cdot \left[(1 - \phi)^2 \boldsymbol{\sigma} \right] = \mathbf{0}$$

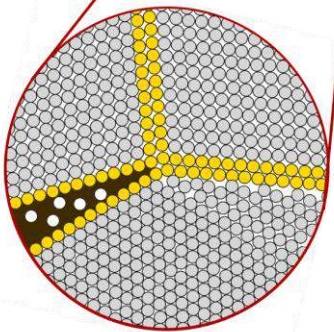
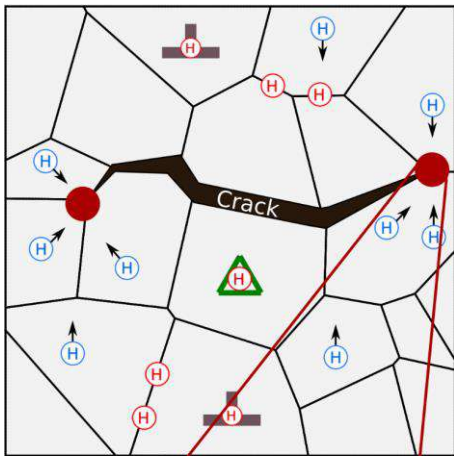
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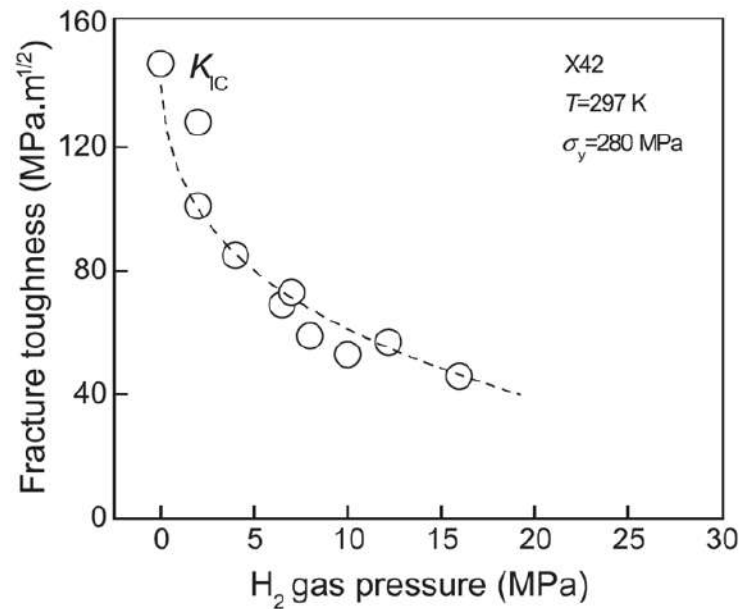
$$G_c(C) \left(\frac{\phi}{\ell} - \ell \nabla^2 \phi \right) - 2(1 - \phi) \psi(\boldsymbol{\epsilon}) = 0$$

Stage III: Fracture



Phase field modelling of H embrittlement

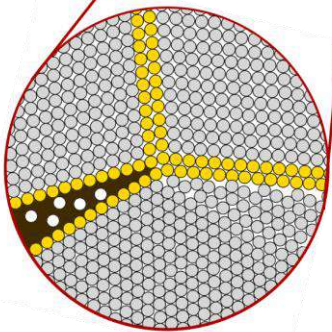
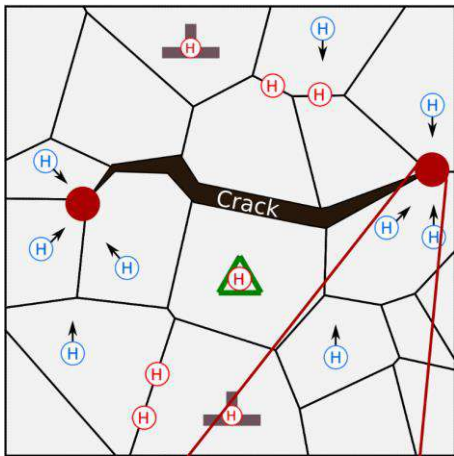
$$G_c(C) \left(\frac{\phi}{\ell} - \ell \nabla^2 \phi \right) - 2(1 - \phi) \psi(\epsilon) = 0$$



Adapted from Gutierrez-Solana F, Elices M. American Society for Metals; 1982

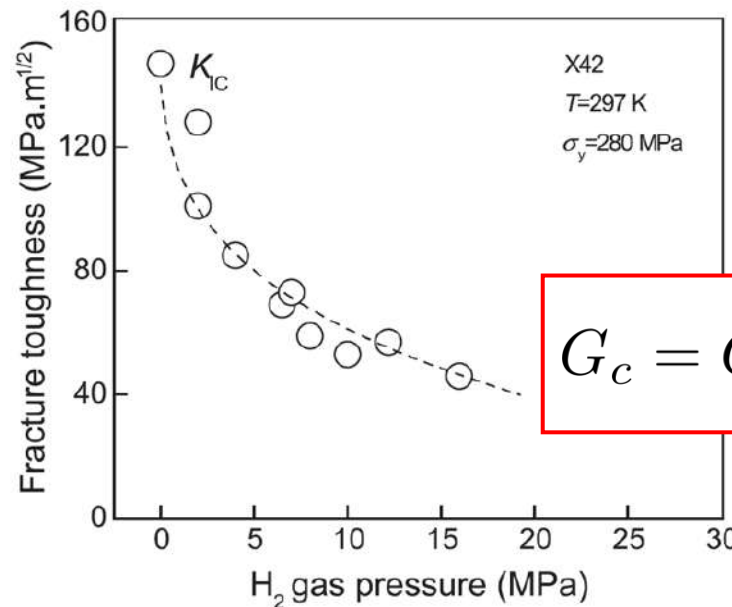
Martínez-Pañeda et al. CMAME (2018)

Stage III: Fracture



Phase field modelling of H embrittlement

$$G_c(C) \left(\frac{\phi}{\ell} - \ell \nabla^2 \phi \right) - 2(1 - \phi) \psi(\epsilon) = 0$$



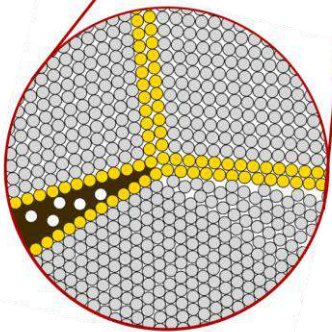
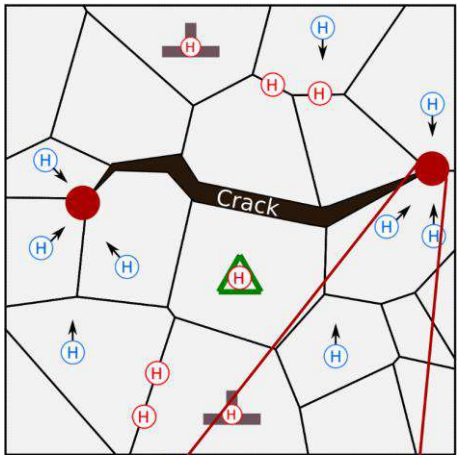
... and the model can accommodate any mechanistic interpretation:

$$G_c = G_c(0) \cdot f \left(C, C_L, C_T, C_T^{gb}, C_T^d, \rho, \epsilon^p, \dots \right)$$

Adapted from Gutierrez-Solana F, Elices M. American Society for Metals; 1982

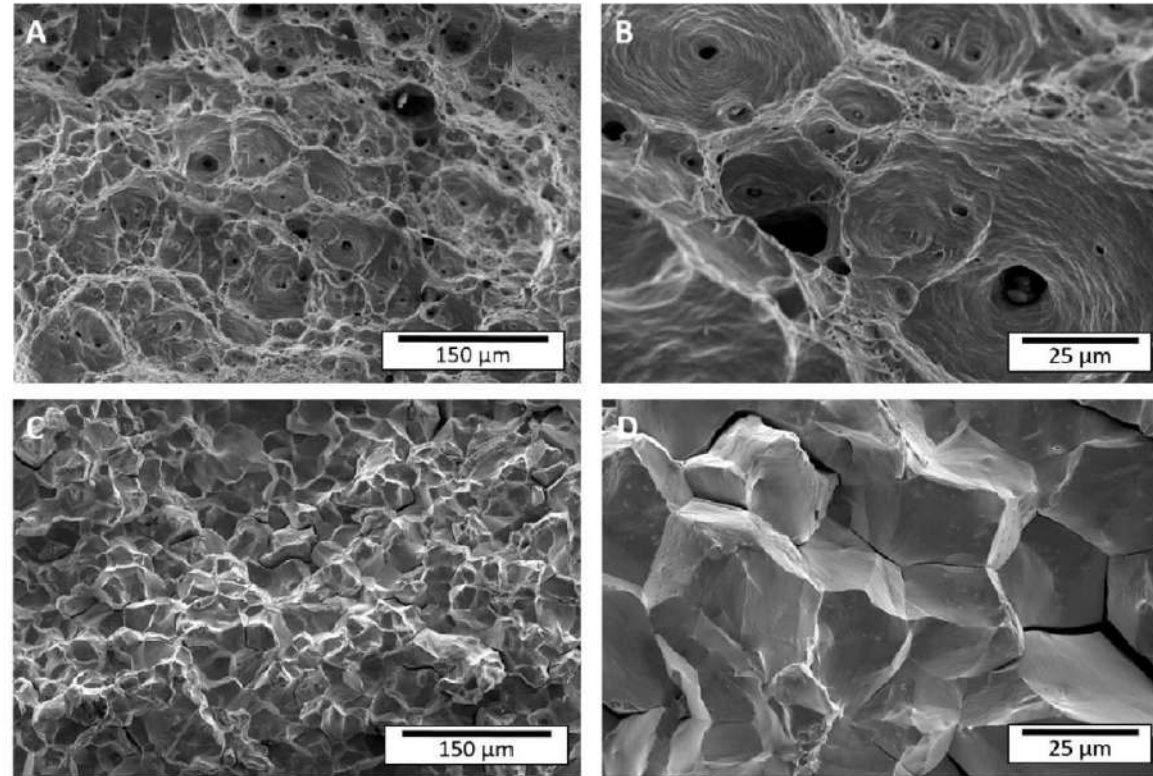
Martínez-Pañeda et al. CMAME (2018)

Stage III: Fracture



Phase field modelling of H embrittlement

- How does hydrogen make metals brittle?

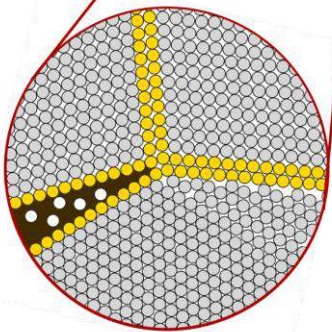
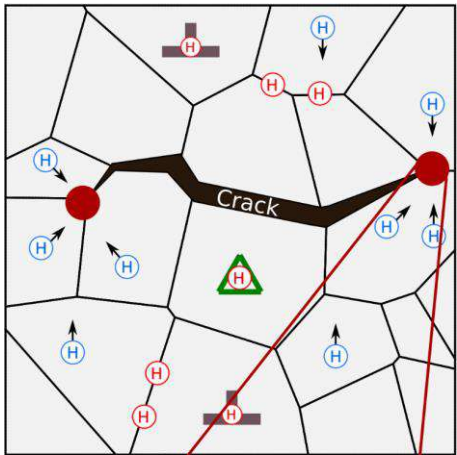


Air

H

Harris et al. (Acta Mat., 2018)

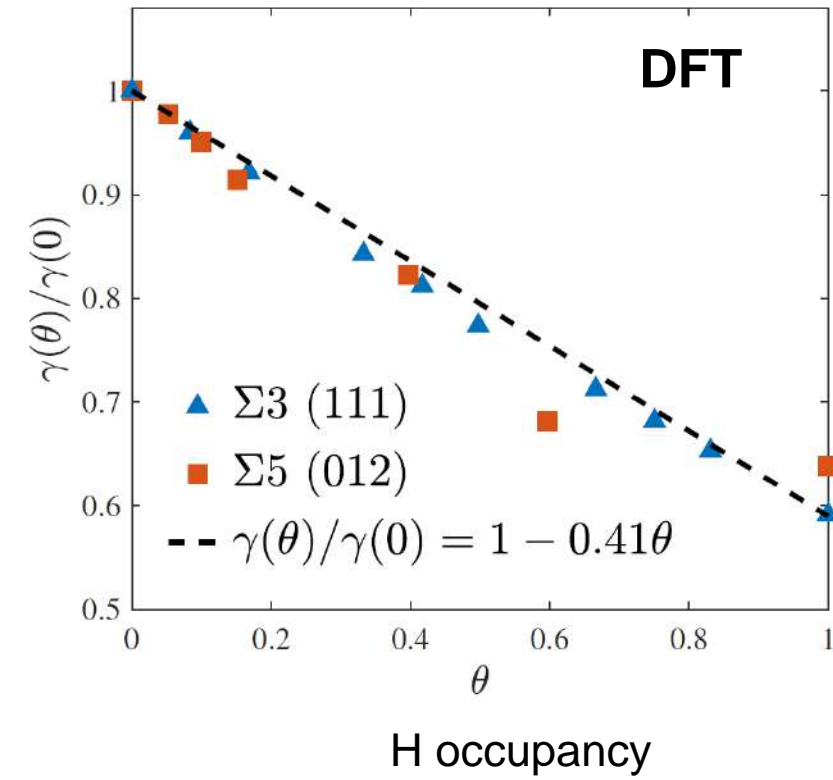
Stage III: Fracture



Phase field modelling of H embrittlement

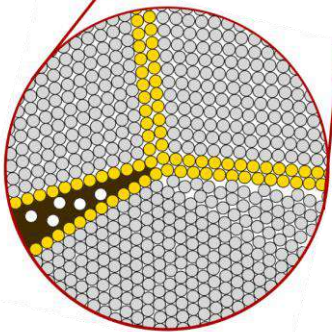
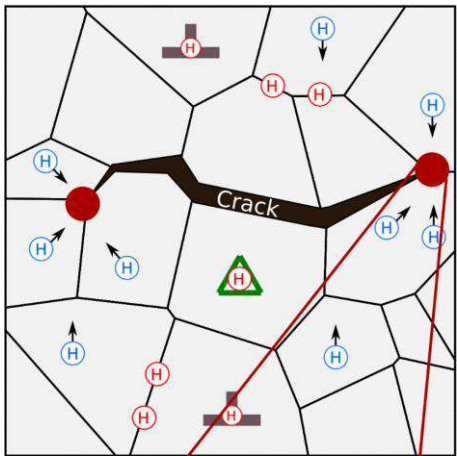
- Hydrogen atoms strongly reduce the bonding strength between metal atoms.

Fracture energy



Alvaro et al. IJHE (2016)

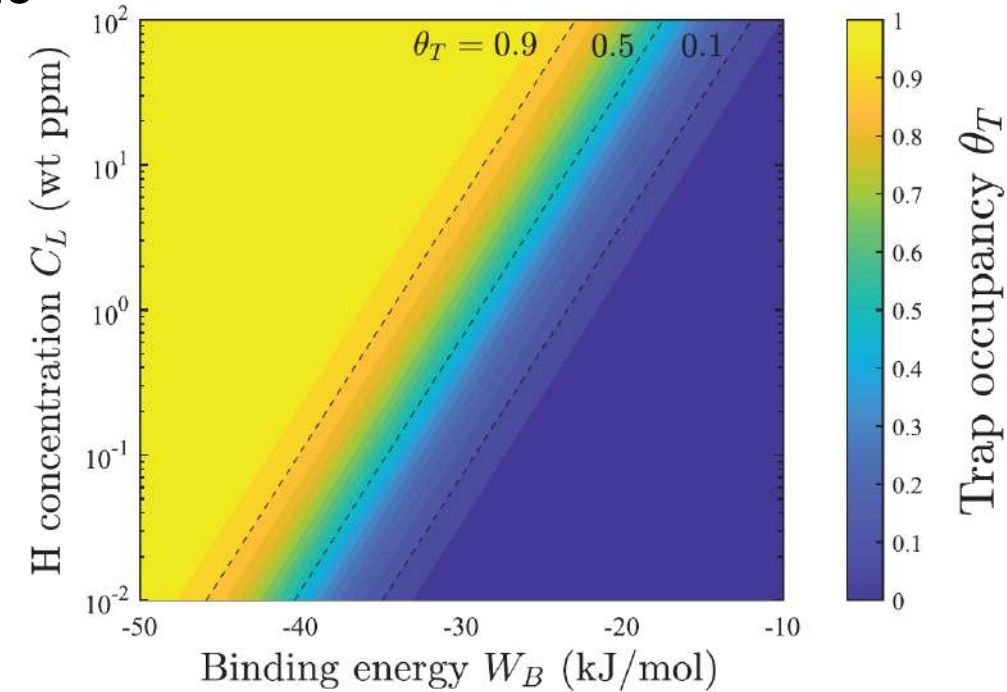
Stage III: Fracture



Phase field modelling of H embrittlement

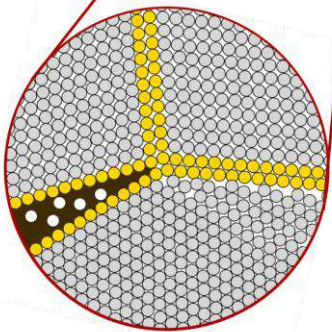
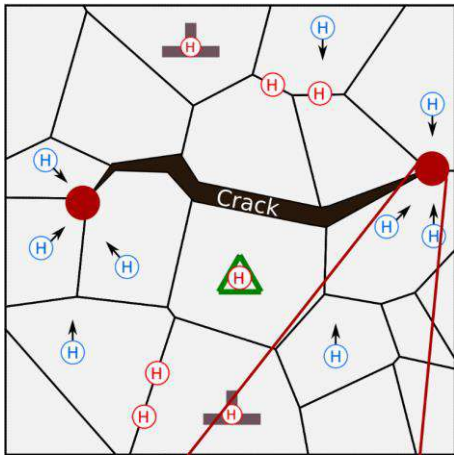
- ❑ Hydrogen atoms strongly reduce the bonding strength between metal atoms.
- ❑ Strong traps ($|W_B| > 40$, like grain boundaries or carbides) are filled soon

Trap occupancy as a function of C_L and W_B (Oriani)



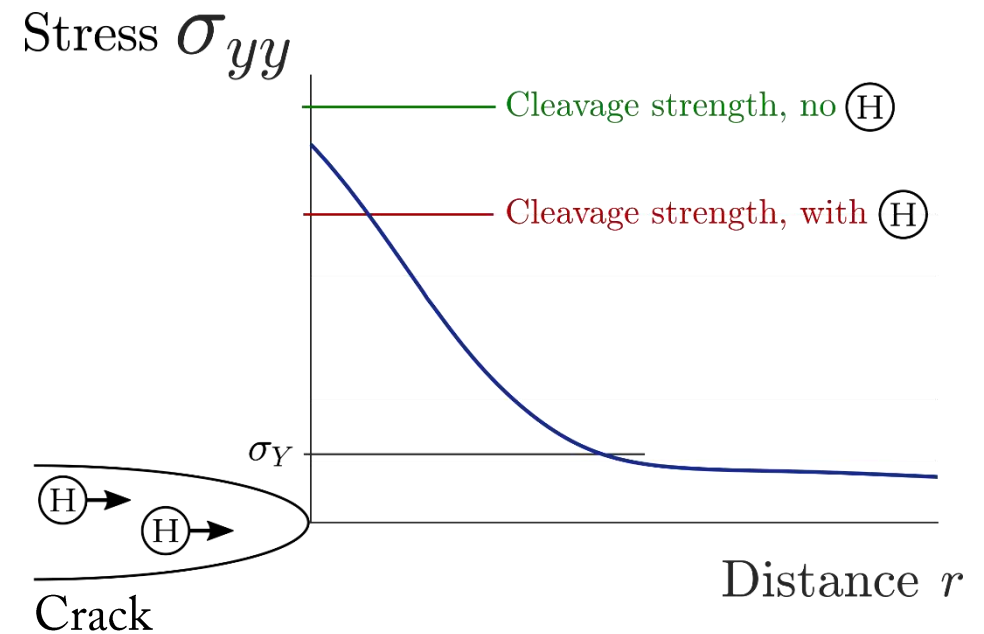
Fernández-Sousa, Betegón, Martínez-Pañeda. *Acta Mat.* (2020)

Stage III: Fracture



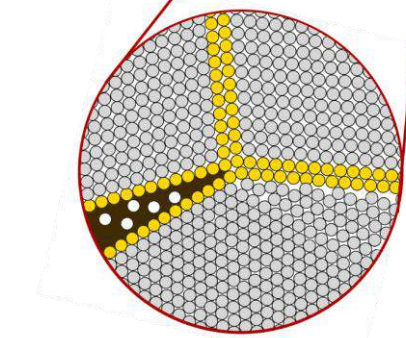
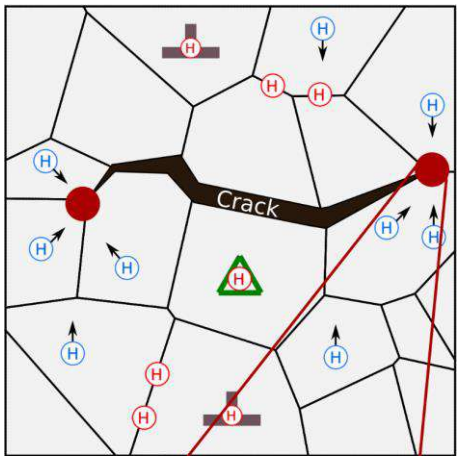
Phase field modelling of H embrittlement

- ❑ Hydrogen atoms strongly reduce the bonding strength between metal atoms.
- ❑ Strong traps ($|W_B| > 40$, like grain boundaries or carbides) are filled soon
- ❑ Gradient-enhanced stresses that are close to the theoretical lattice (or GB) strength ($\hat{\sigma} > 10\sigma_Y$)



Martínez-Pañeda et al., *JMPS* (2019)

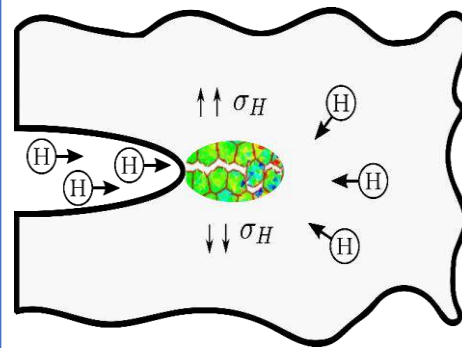
Stage III: Fracture



Phase field modelling of H embrittlement

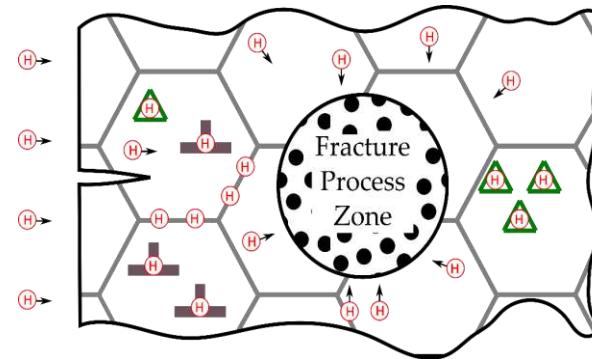
$$G_c(C) \left(\frac{\phi}{\ell} - \ell \nabla^2 \phi \right) - 2(1 - \phi) \psi_0(\epsilon) = 0$$

Stress-assisted diffusion



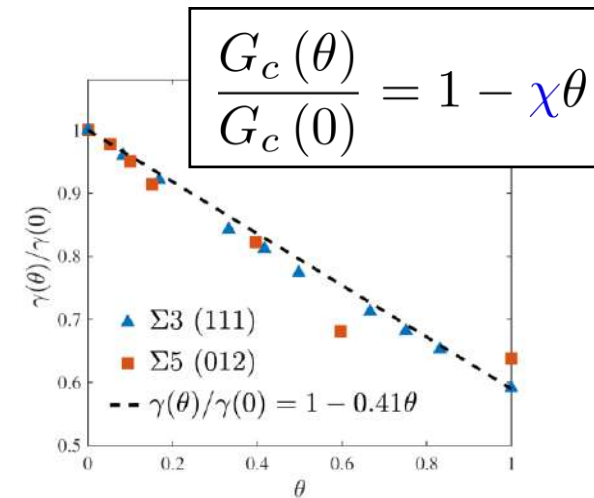
Lattice hydrogen concentration C_L

Trapping thermodynamics

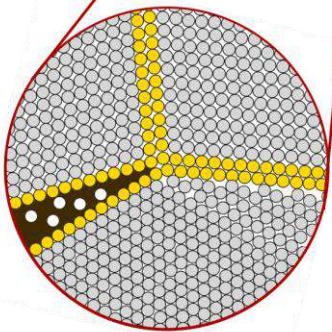
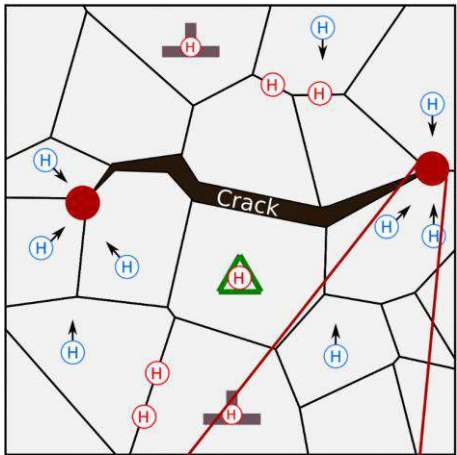


Trap occupancy θ

Atomistic calculations



Stage III: Fracture



Phase field modelling of H embrittlement

☐ *Moving* chemical boundary conditions



ϕ - Crack phase field

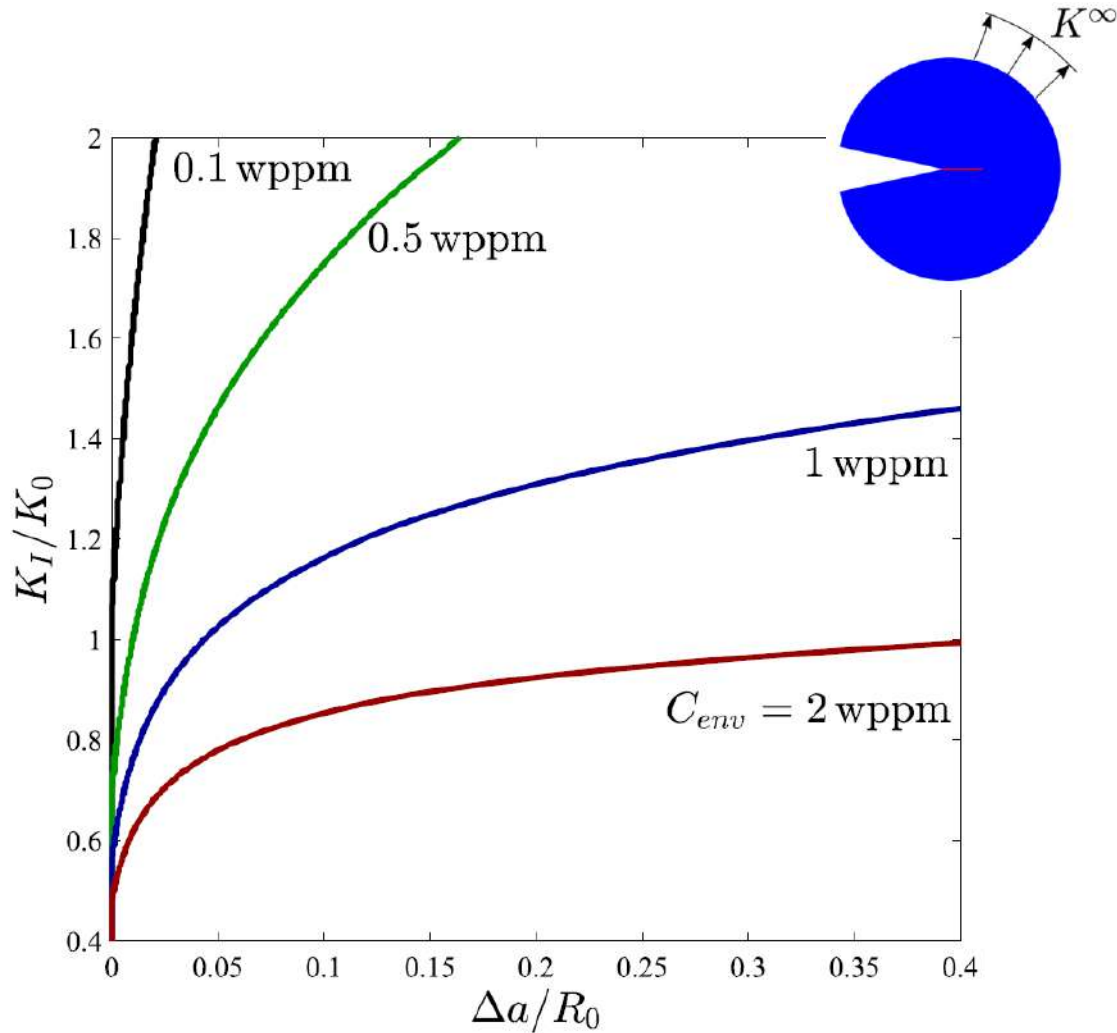
red – cracked material

blue – intact material

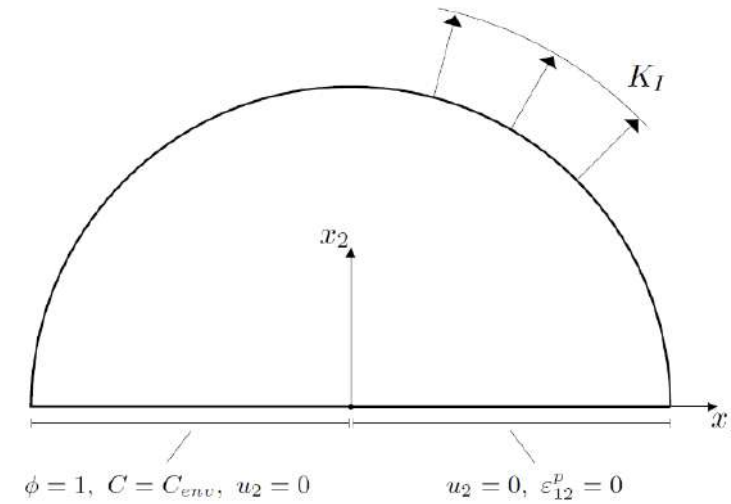
C - H concentration

Kristensen et al., *JMPS* (2020)

Results: R-curves



□ Influence of the H content

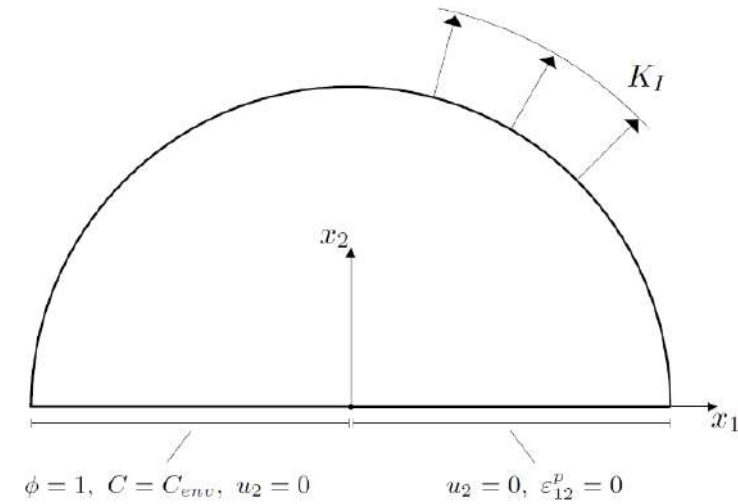
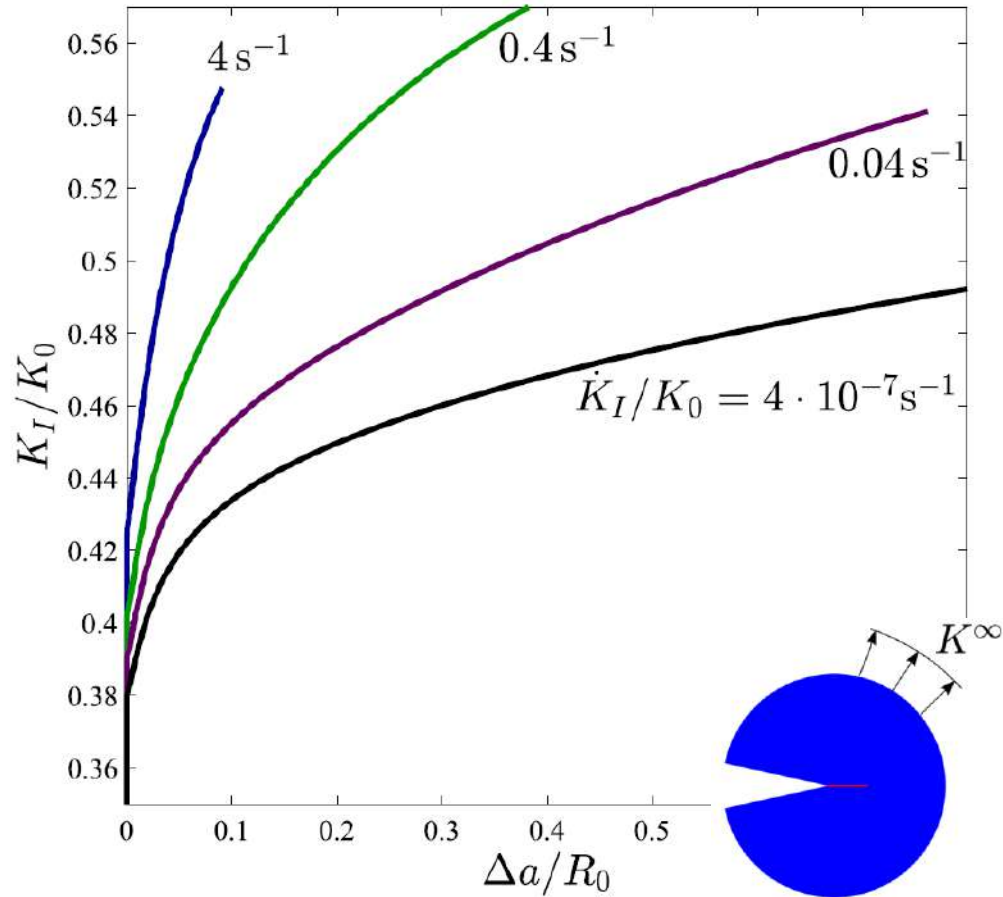


$$K_0 = \sqrt{\frac{EG_c}{1 - \nu^2}} \quad R_0 = \frac{1}{3\pi(1 - \nu^2)} \frac{G_c E}{\sigma_y^2}$$

Kristensen, Niordson, Martínez-Pañeda. *JMPS* (2020)

Results: R-curves

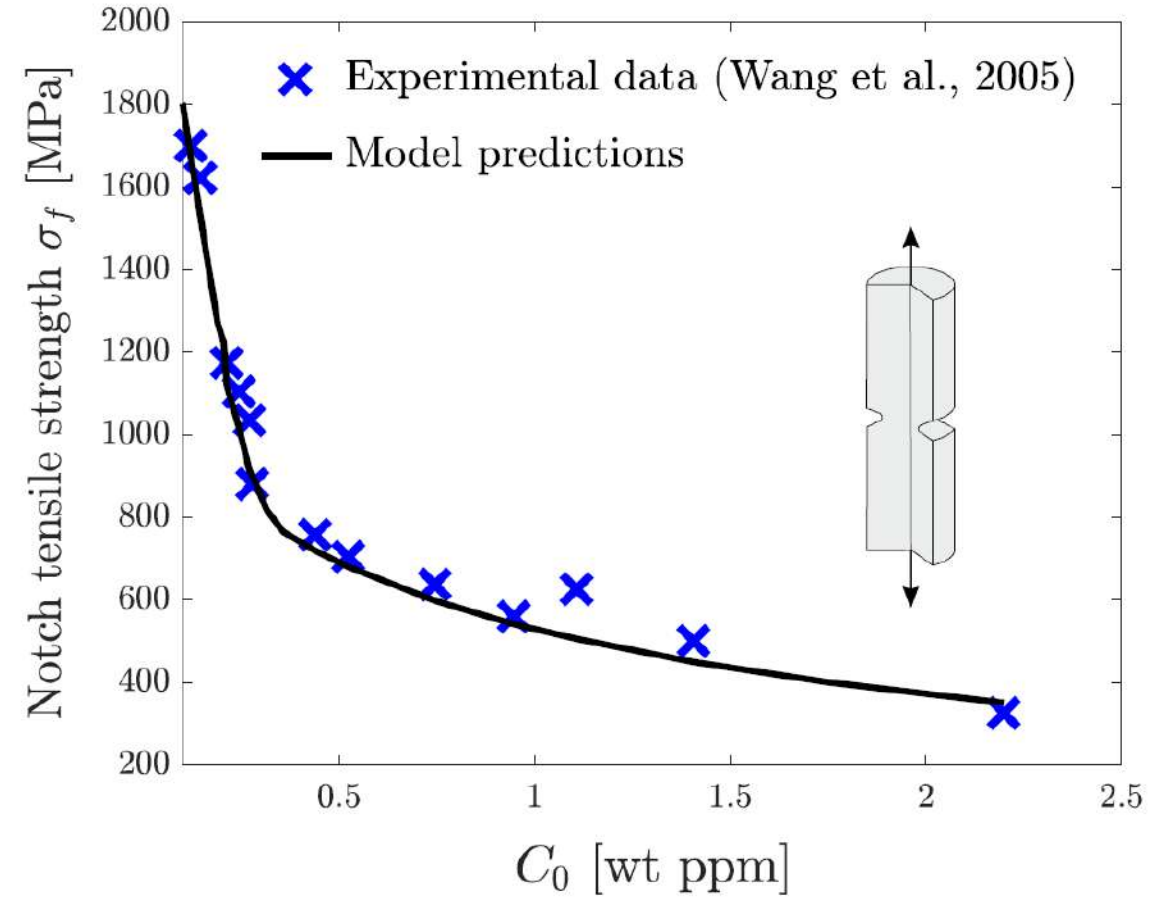
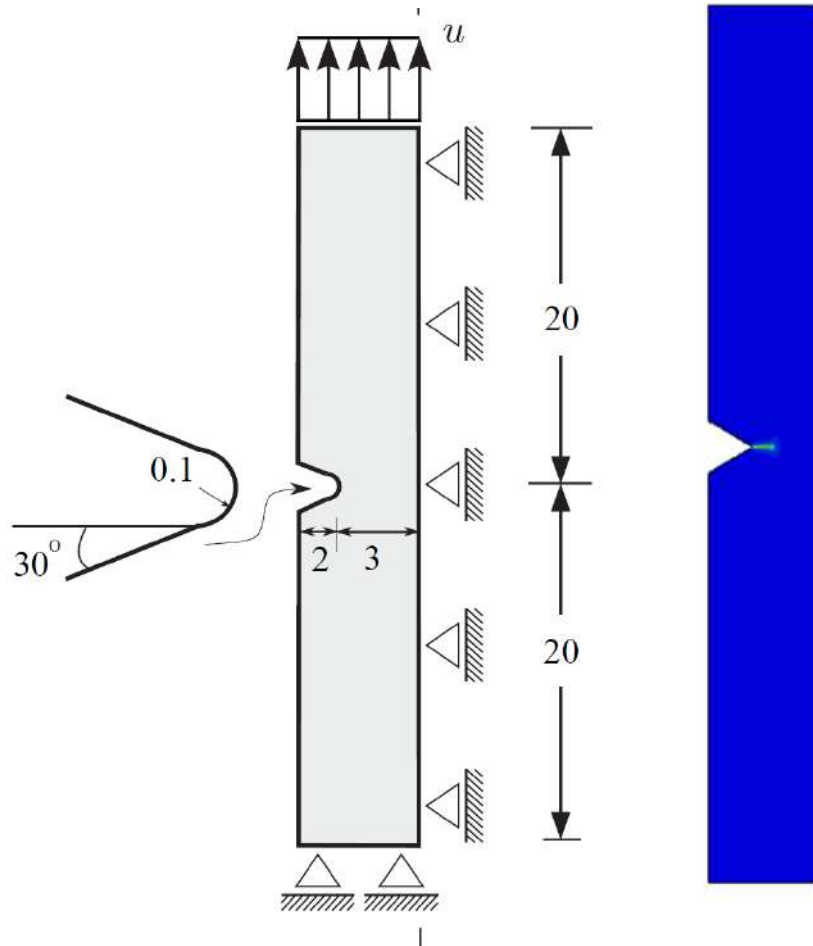
- Influence of the loading rate



$$K_0 = \sqrt{\frac{EG_c}{1 - \nu^2}} \quad R_0 = \frac{1}{3\pi(1 - \nu^2)} \frac{G_c E}{\sigma_y^2}$$

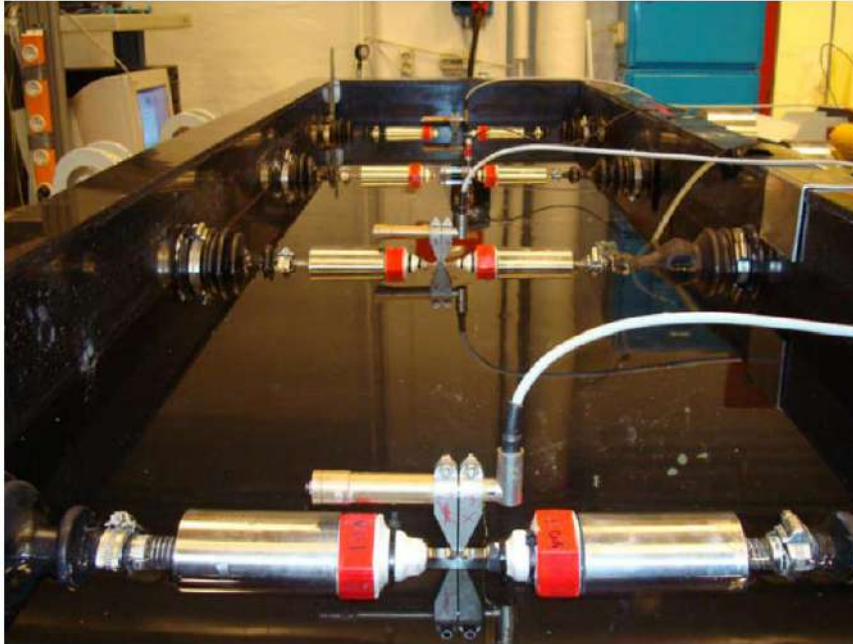
Kristensen, Niordson, Martínez-Pañeda. *JMPS* (2020)

Results: pre-charged steel bars

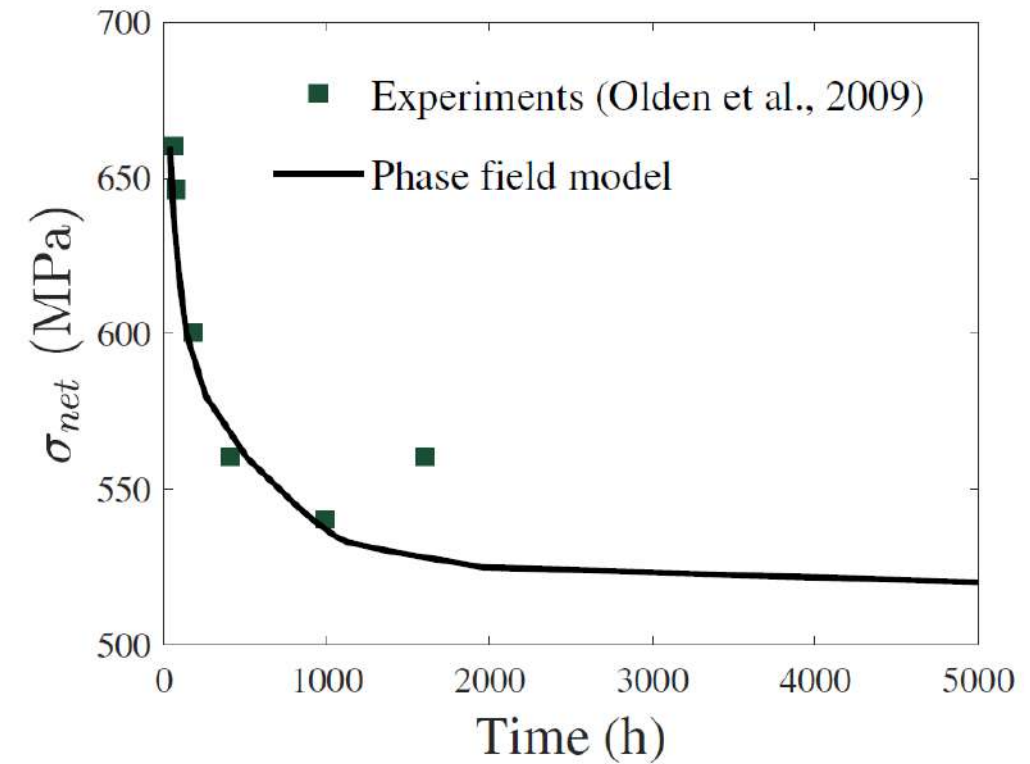


Isfandbod & Martínez-Pañeda. *Int. J. Plasticity* (2021)

Results: steel samples at constant load



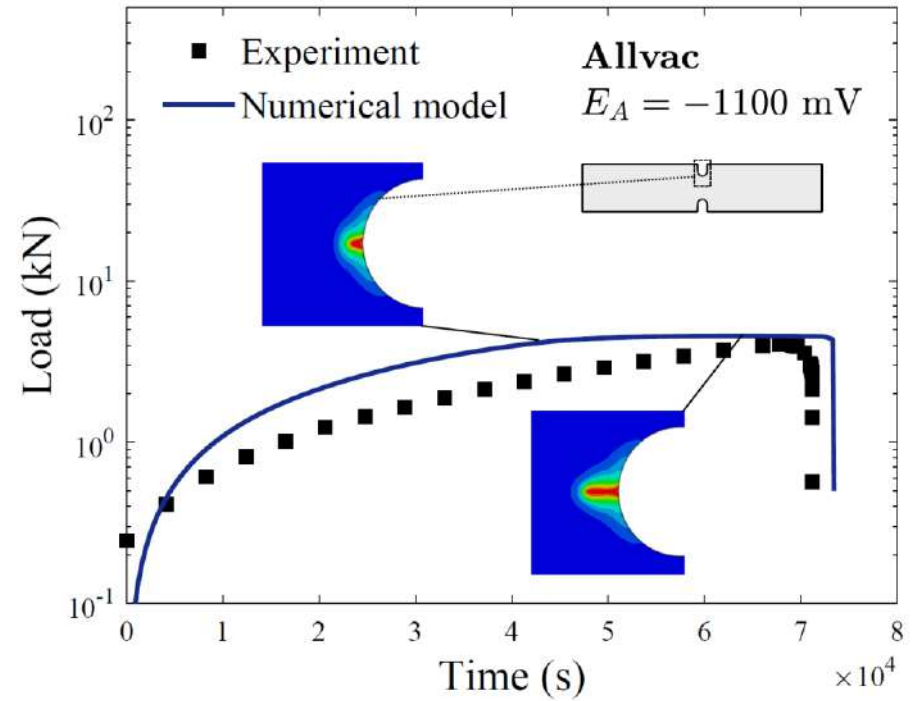
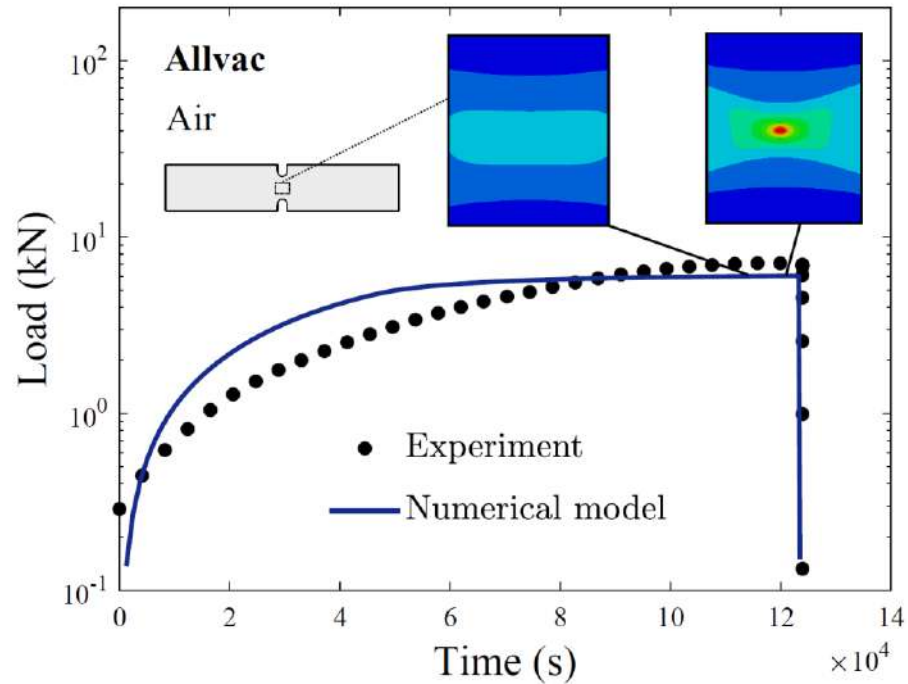
SINTEF



- ✓ Virtual experiments enable predictions over large time scales

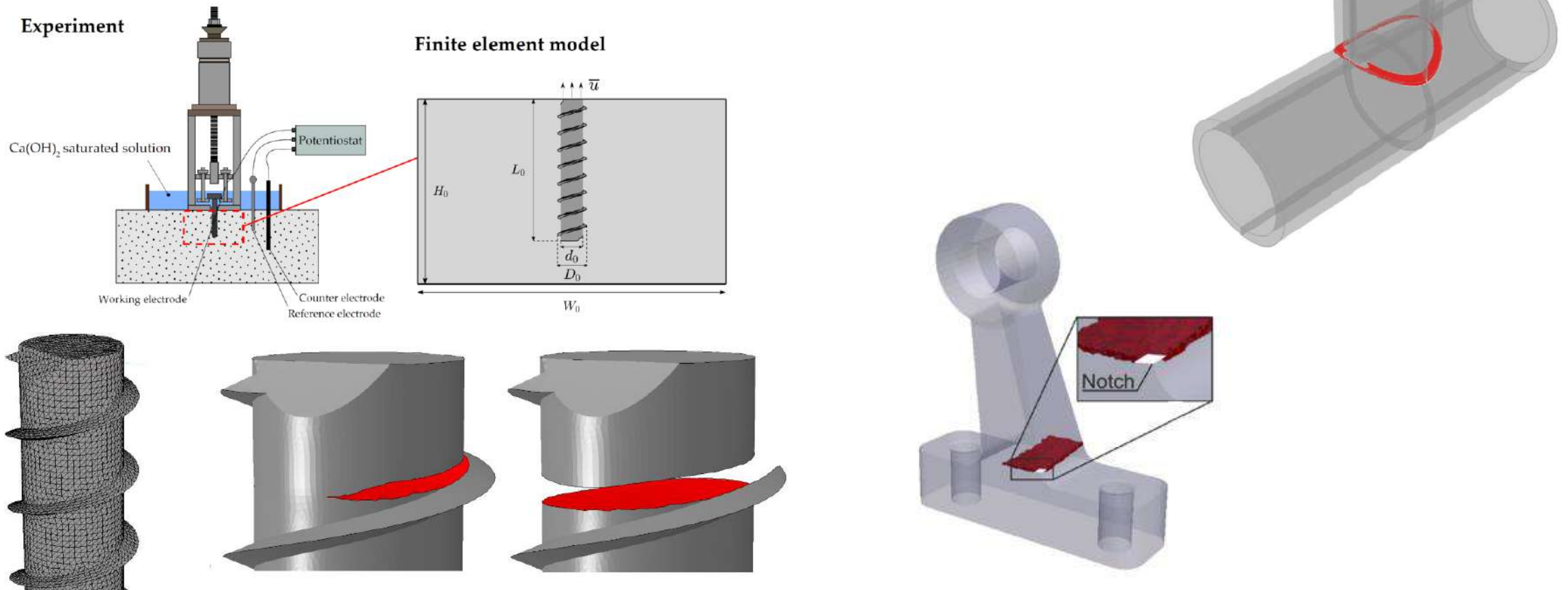
Martínez-Pañeda et al., *CMAME* (2018)

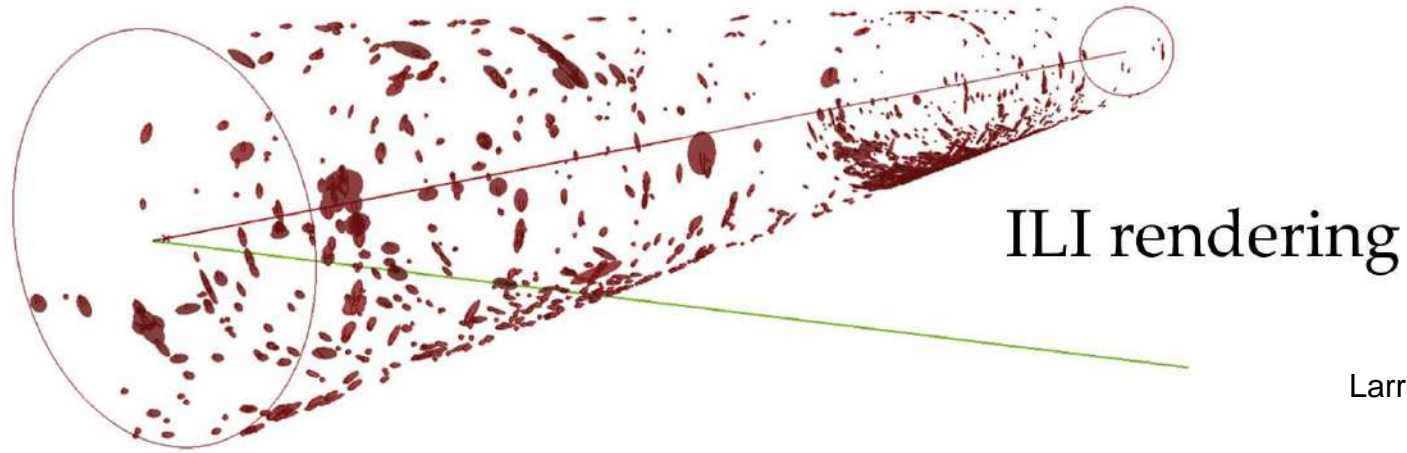
Results: are SSRT experiments suitable?



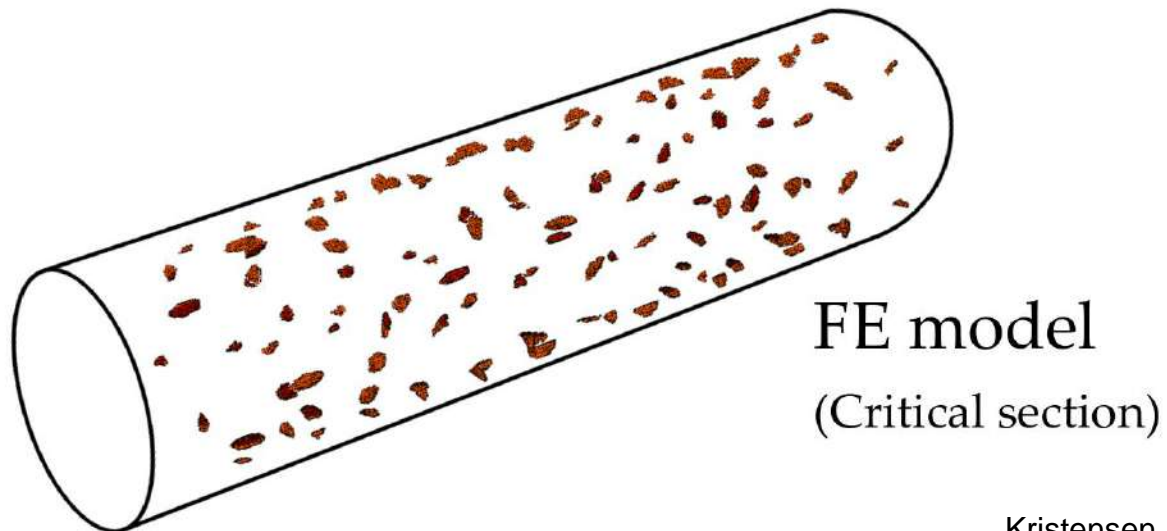
- Early cracking occurs in SSRTs – time to failure is not a valid measure

ASTM E488: SCC Strength of Anchors in Concrete

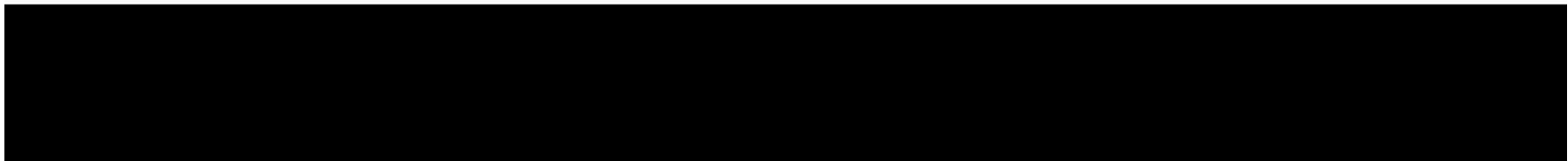
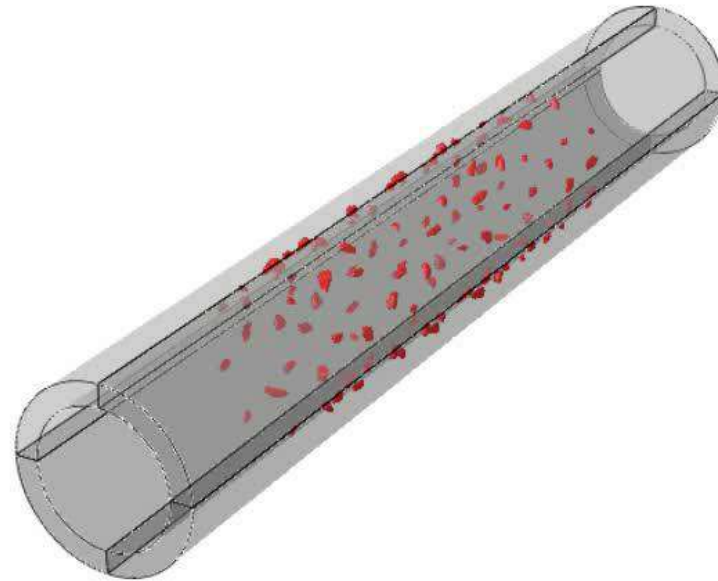
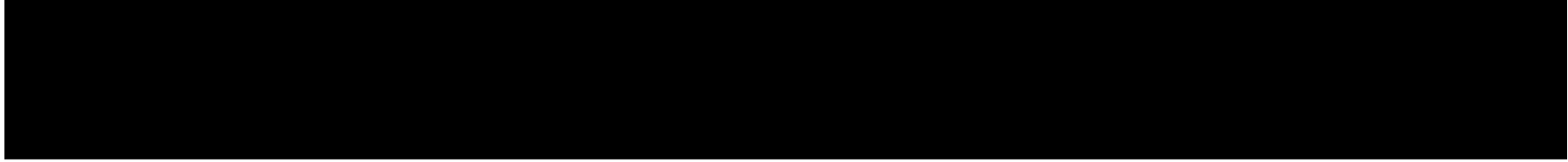




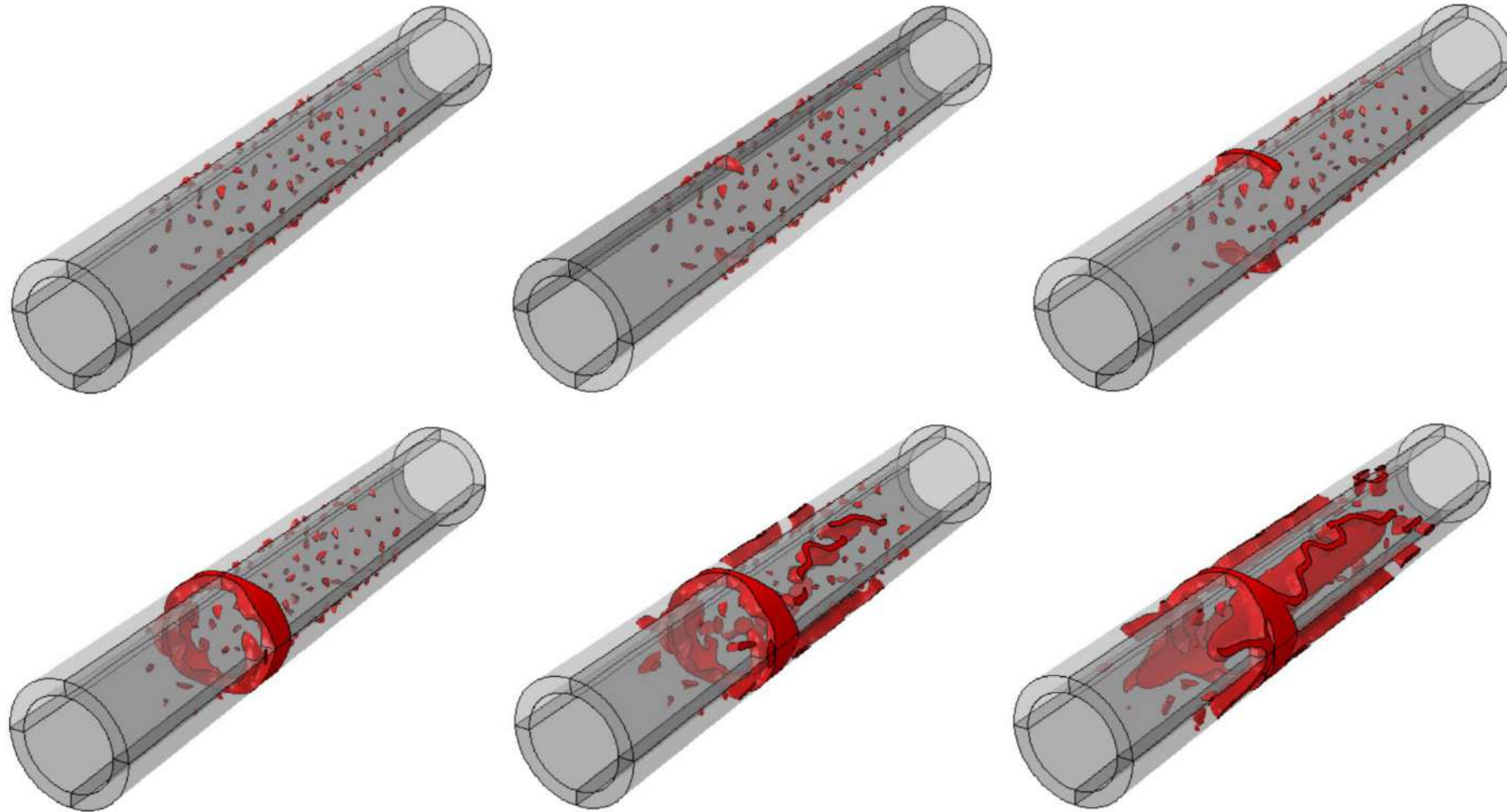
Larrosa et al. *Theor. Appl. Fract. Mech.* (2018)



Kristensen, Niordson, Martínez-Pañeda. *Theor. Appl. Fract. Mech.* (2020)



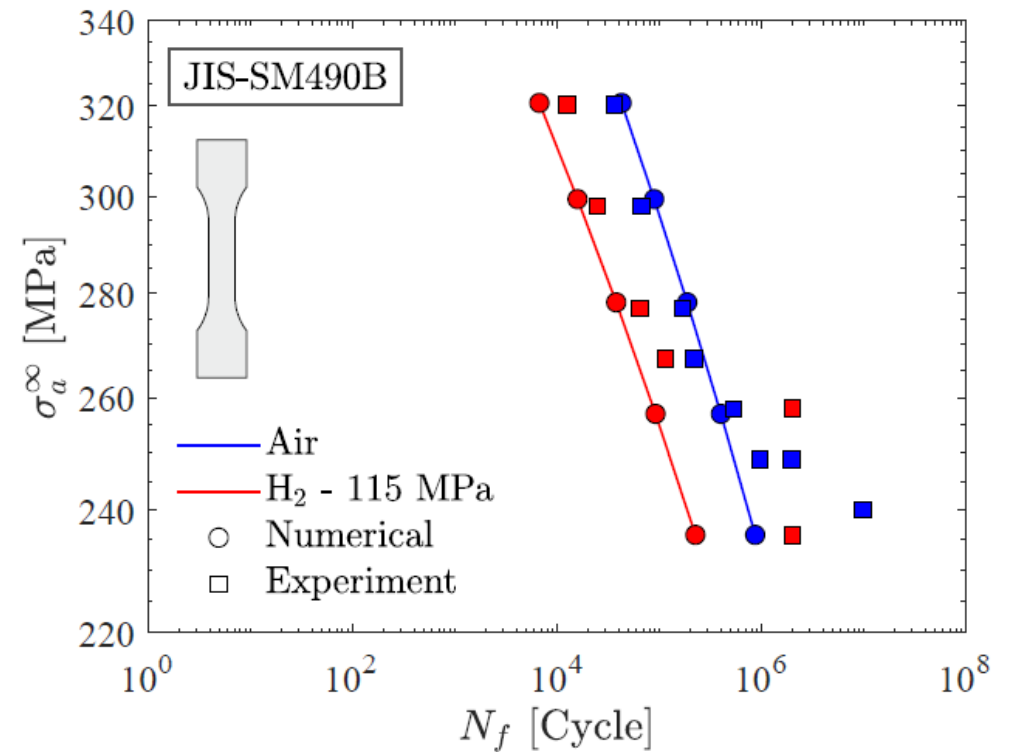
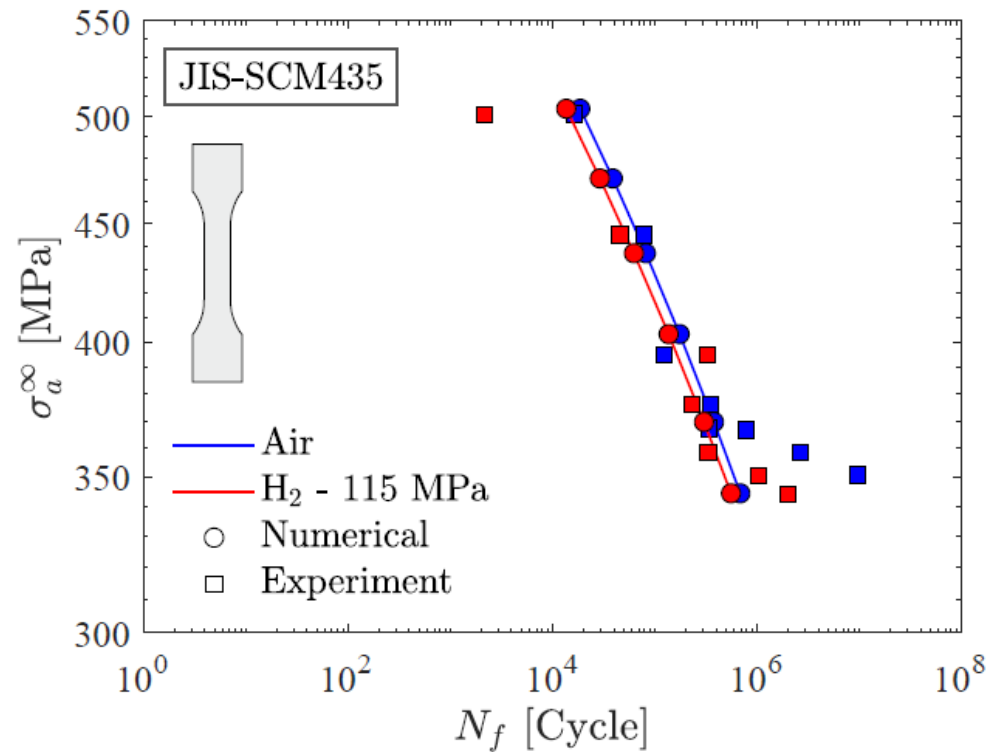
Results: *Virtual Testing*



Kristensen, Niordson, Martínez-Pañeda. *Theor. Appl. Fract. Mech.* (2020)

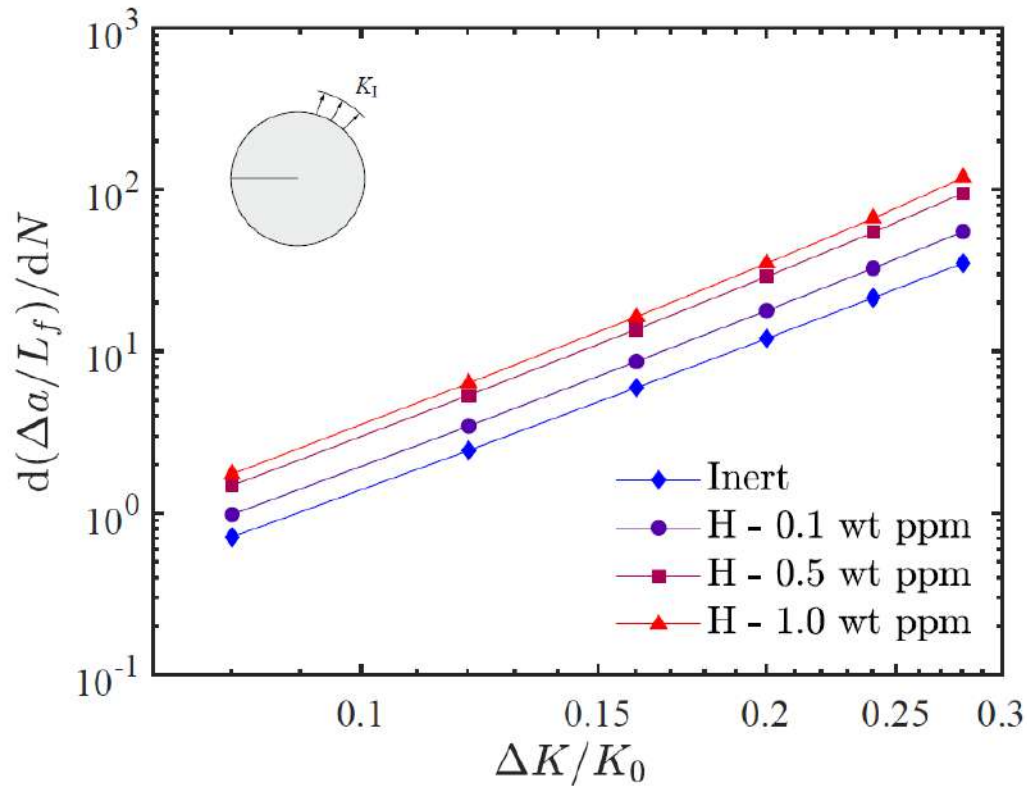
Results – Hydrogen-assisted Fatigue

$$f(\bar{\alpha}(t))G_c(C) \left(\frac{\phi}{\ell} - \ell \nabla^2 \phi \right) - 2(1 - \phi) \psi(\epsilon) = 0 \quad \text{in } \Omega$$

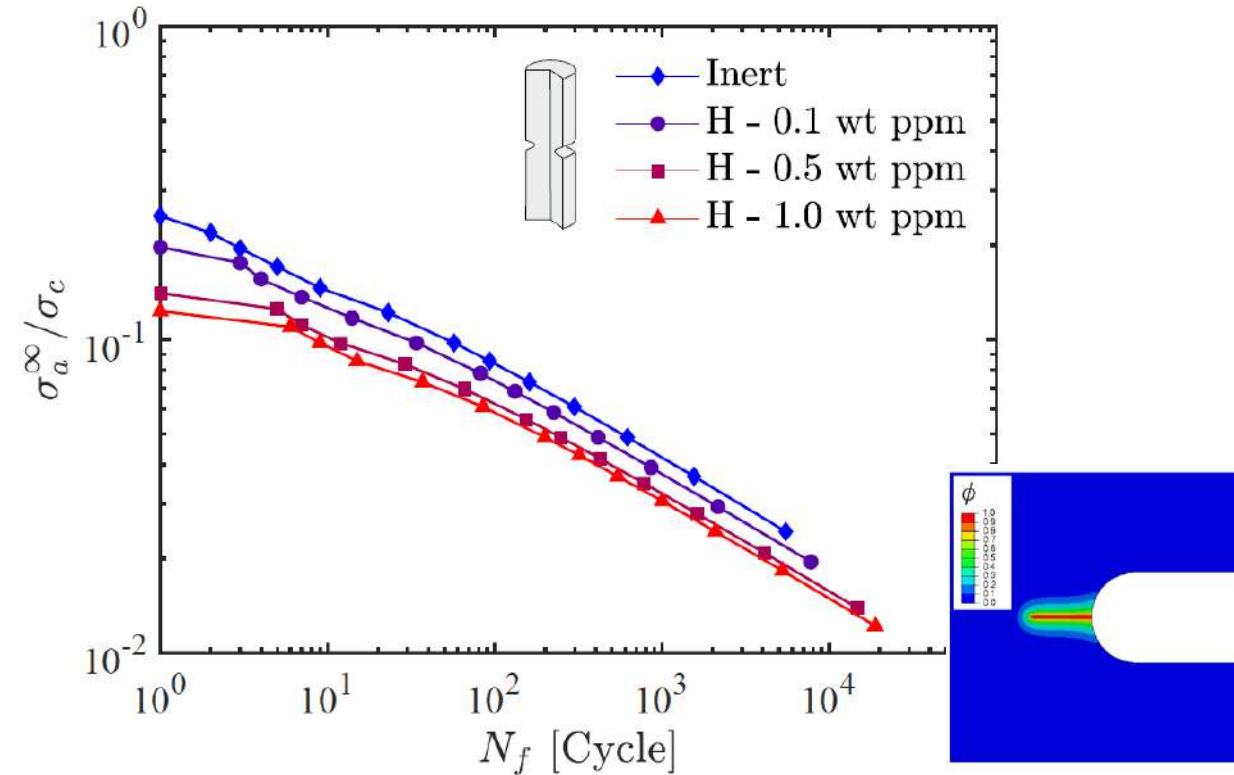


Golahmar, Kristensen, Niordson, Martínez-Pañeda. *Int. J. Fatigue* (2022)

Paris law behaviour



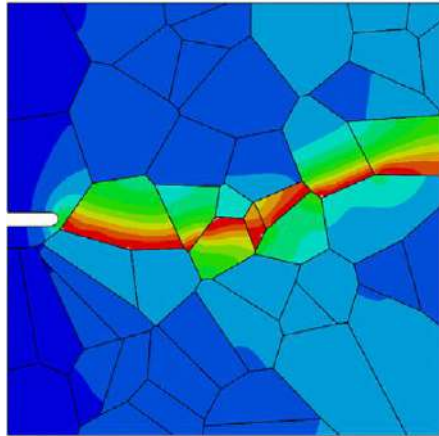
Virtual S-N curves



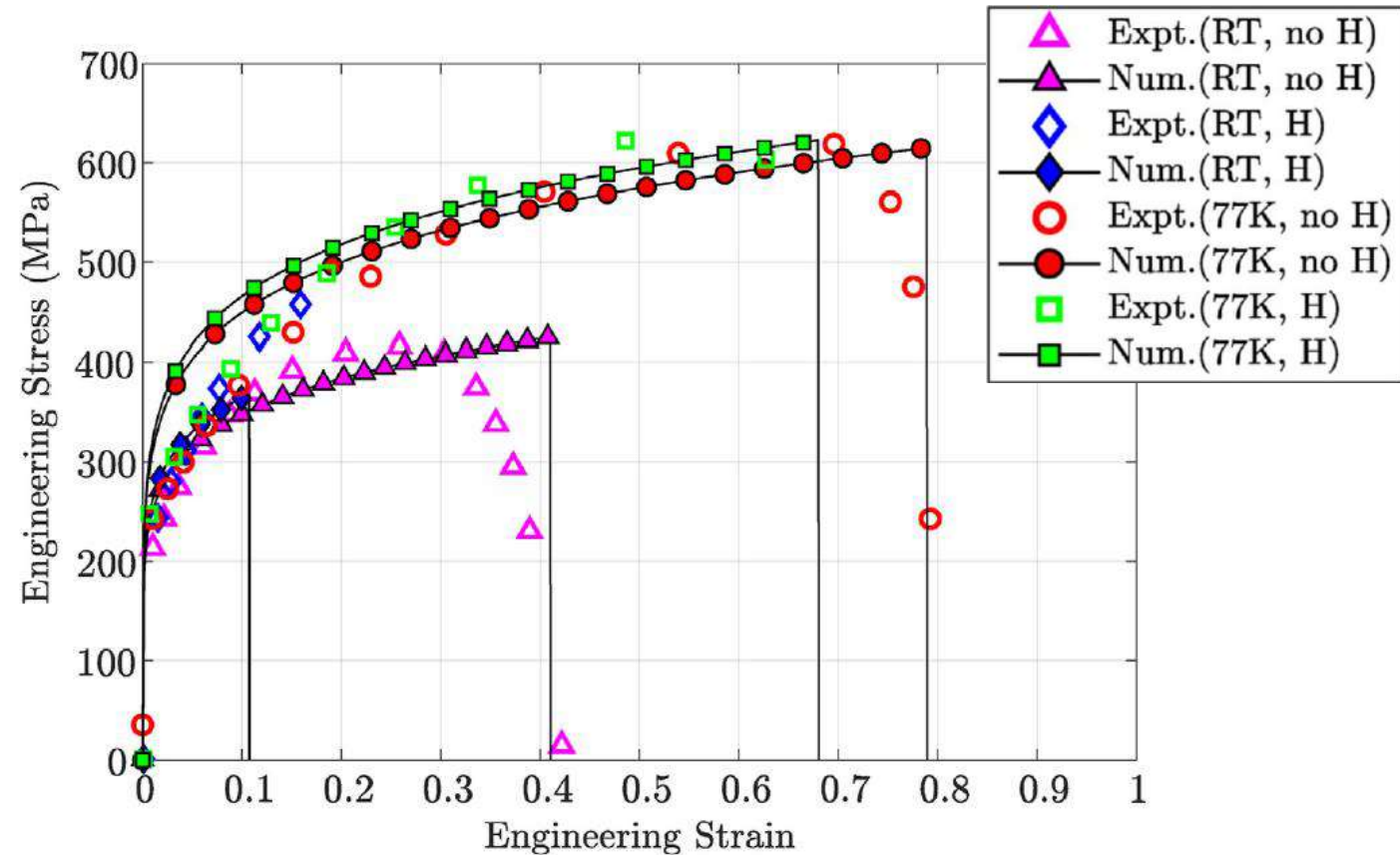
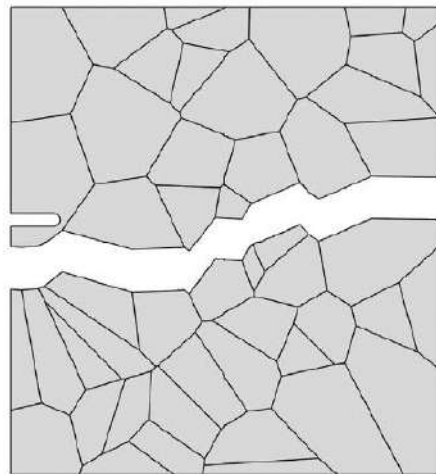
Golahmar, Kristensen, Niordson, Martínez-Pañeda. *Int. J. Fatigue* (2022)

Results – Intergranular cracking

Phase field:
Ductile transgranular cracking

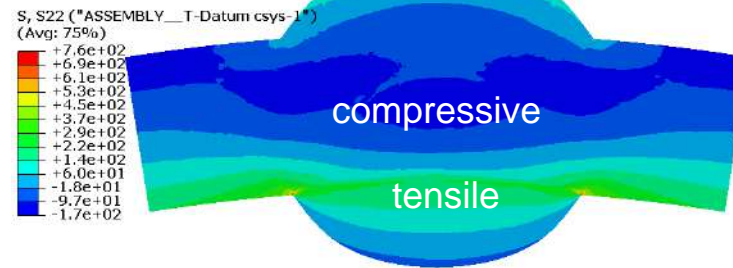
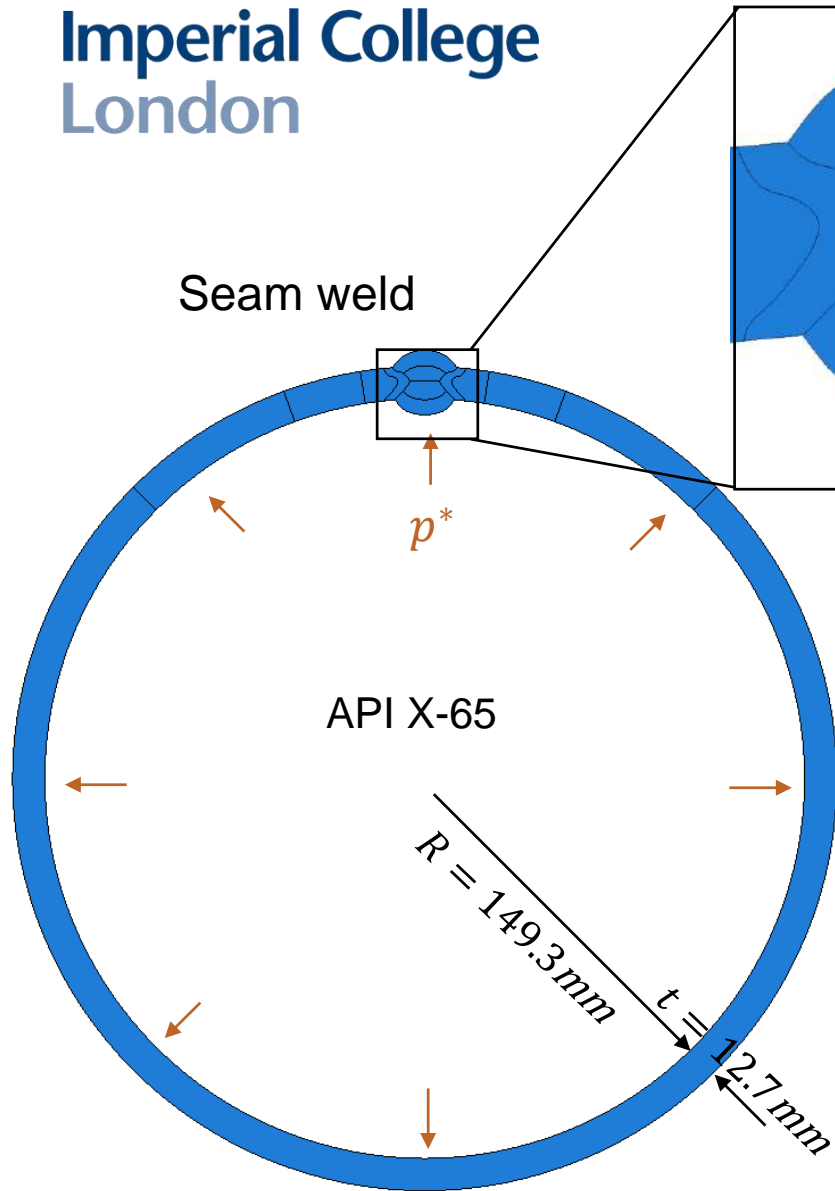


Cohesive zone model:
Brittle intergranular cracking

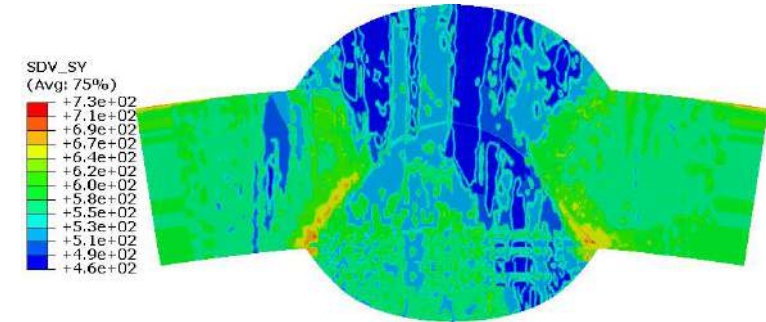


Valverde-González, Martínez-Pañeda *et al.* *Int. J. Hydrogen Energy* (2022)

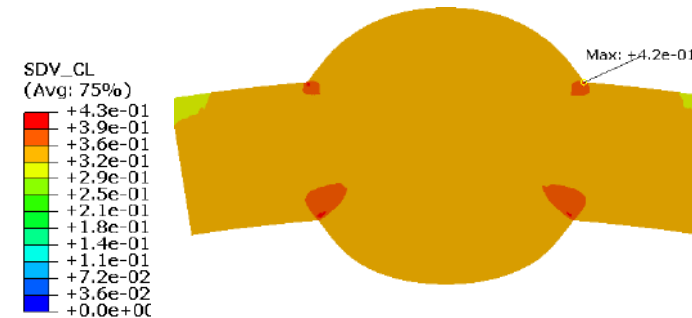
Results – Welded joints



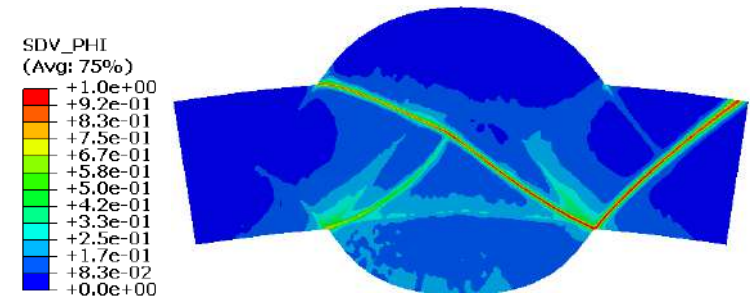
Residual stresses



Microstructural variation



Hydrogen distribution

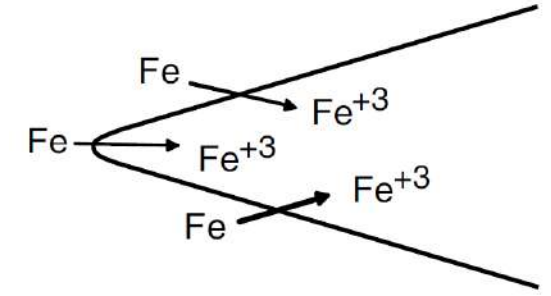
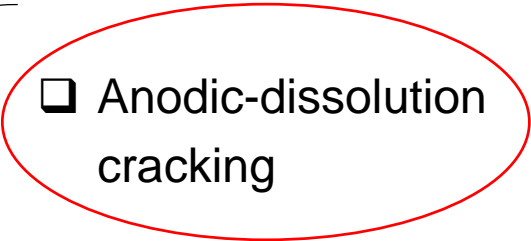


Cracking

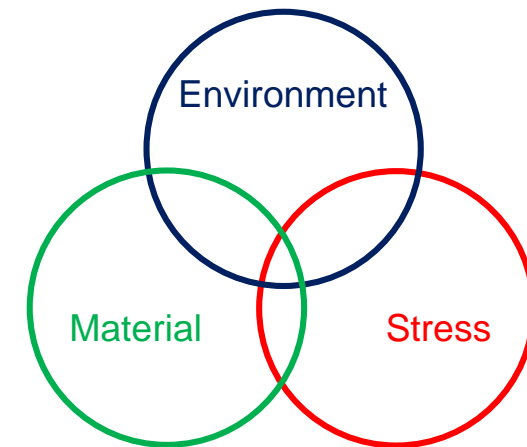
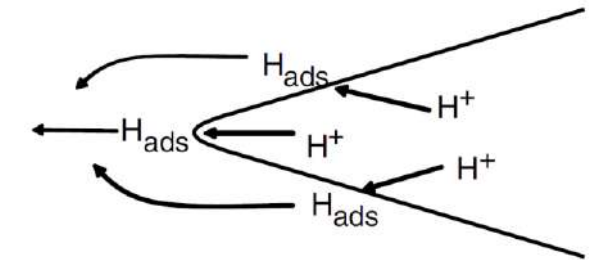
Castro et al. (in preparation)
Mandal et al. (in preparation)

Environmentally
assisted cracking

- Stress Corrosion Cracking (SCC)
- Anodic-dissolution cracking
- Hydrogen embrittlement
- Hydrogen embrittlement
- Liquid Metal Embrittlement
- Oxidation fatigue, *etc.*



Hydrogen embrittlement



Corrosion – everyone’s problem

- Massive societal cost: Globally, US\$2.5 trillion per year
- Biggest threat to the durability and sustainability of materials
- Often resulting in catastrophic failures
- Long-standing scientific and technological challenge



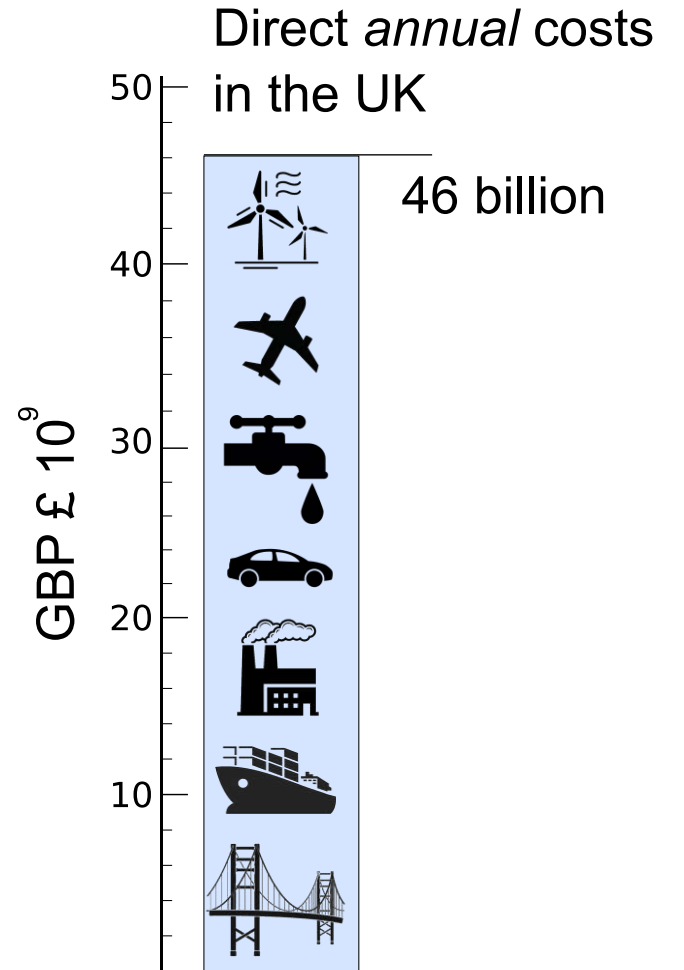
Morandi bridge collapse (Italy)



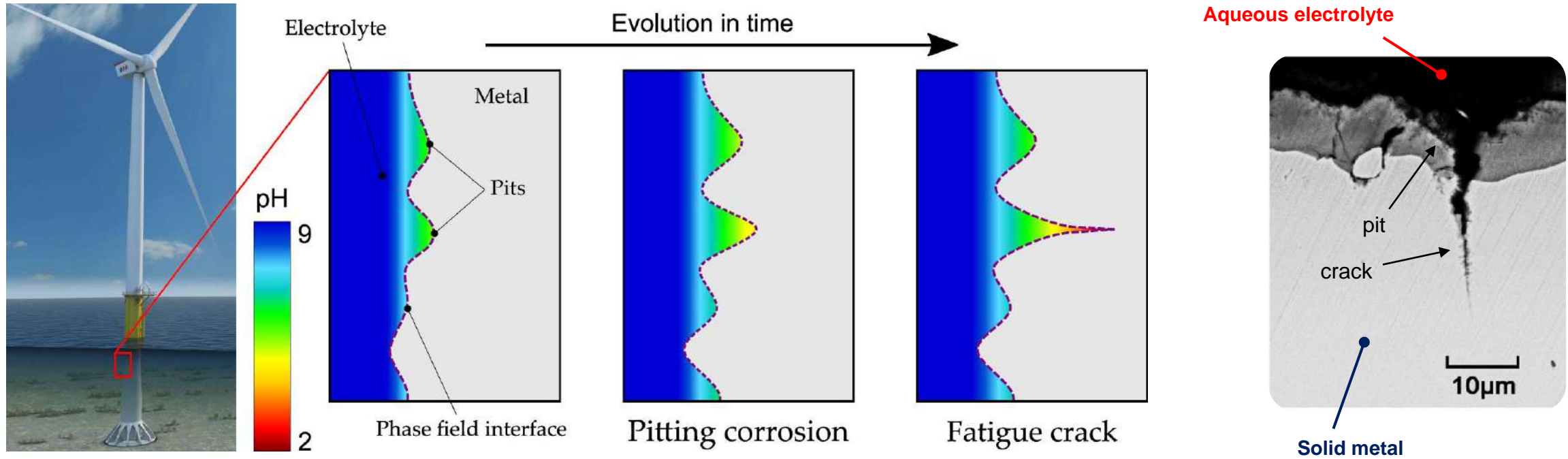
Prestige disaster (Spain)



FedEx landing gear failure (FLL airport)

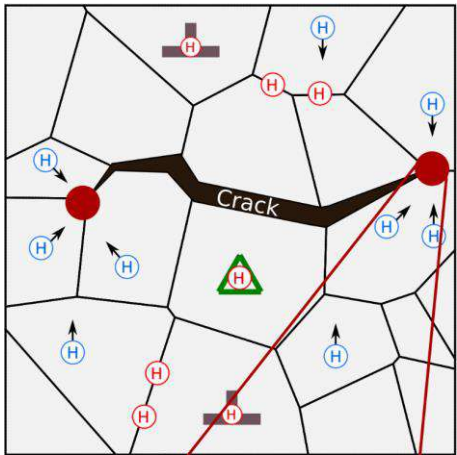


A new phase field paradigm: corrosion

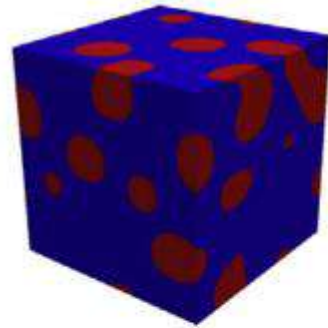


Martínez-Pañeda (RILEM Technical Letters, 2021)

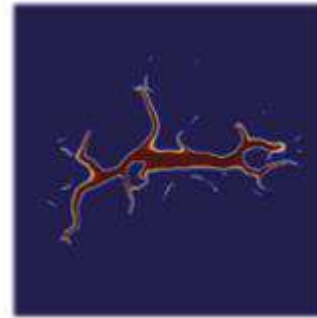
Stage III: Fracture



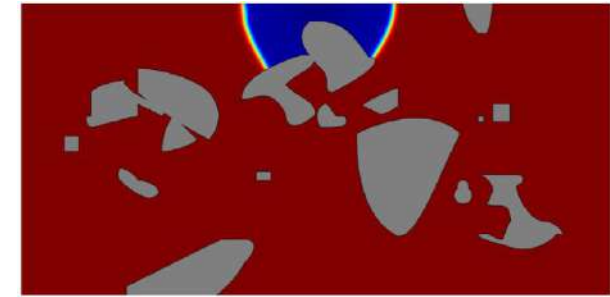
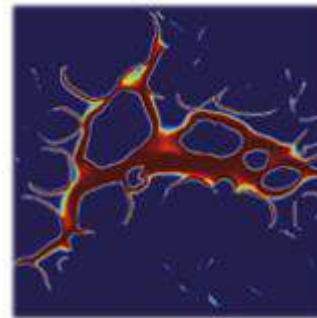
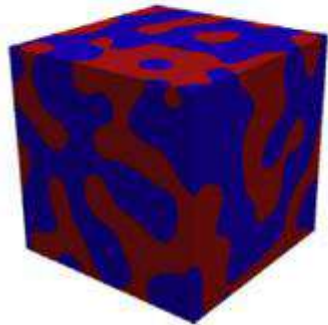
Phase field modelling



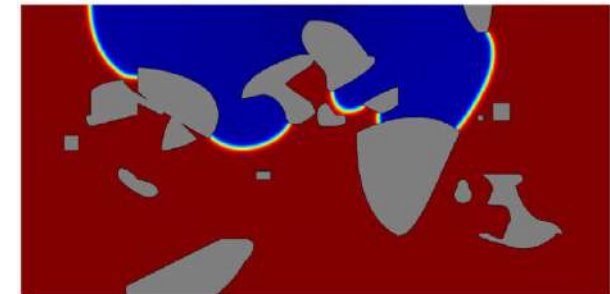
Microstructural evolution



Fracture mechanics



t_0

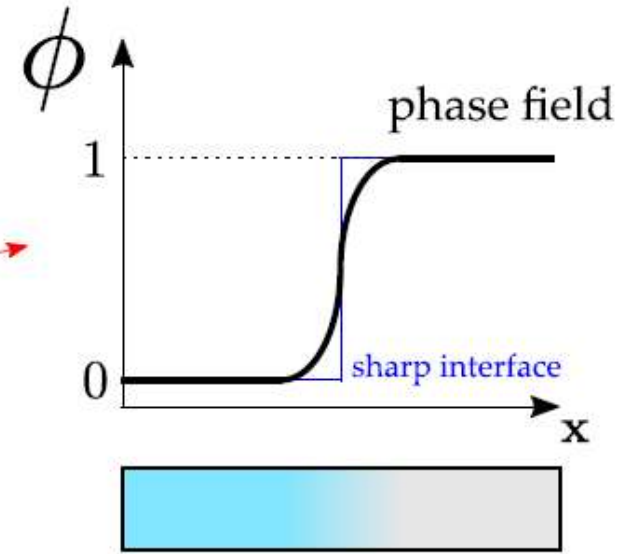
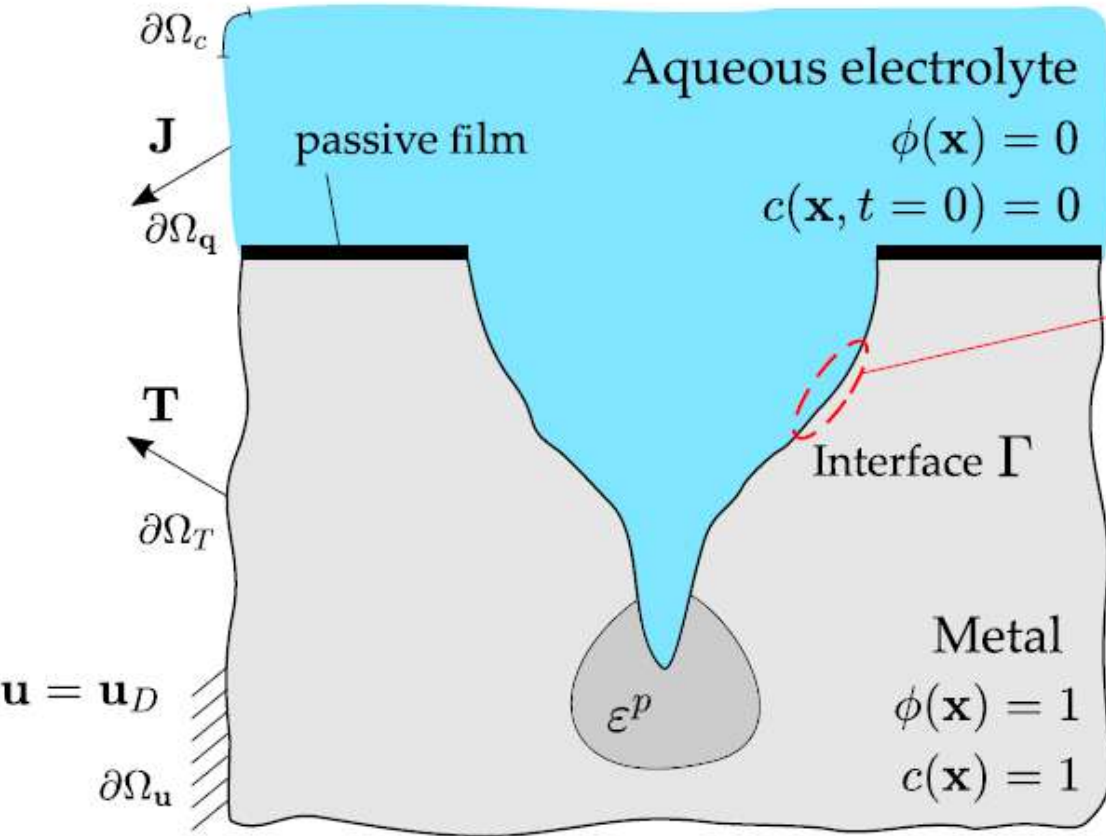


t_1

Corrosion

Kristensen, Niordson, Martínez-Pañeda. *Philosophical Transactions of the Royal Society A* (2021)

A new phase field paradigm: corrosion



$$\frac{\partial \phi}{\partial t}(\mathbf{x}, t) = -L \left(\frac{\partial f}{\partial \phi} - \alpha \nabla^2 \phi \right)$$

$$\frac{\partial c}{\partial t}(\mathbf{x}, t) = \nabla \cdot M \left(\nabla \frac{\partial f}{\partial c} \right)$$

Cui, Ma, Martínez-Pañeda. *JMPS* (2021)

Phase field evolution (interface reaction)

$$\frac{\partial \phi}{\partial t}(\mathbf{x}, t) = -L \left(\frac{\partial f}{\partial \phi} - \alpha \nabla^2 \phi \right)$$

$$\frac{d\phi}{dt} + L \left(-2A [c - h(\phi)(c_{Se} - c_{Le}) - c_{Le}] (c_{Se} - c_{Le}) h'(\phi) + wg'(\phi) - \alpha \nabla^2 \phi \right) = 0$$

Concentration of metal ions

$$\frac{\partial c}{\partial t}(\mathbf{x}, t) = \nabla \cdot M \left(\nabla \frac{\partial f}{\partial c} \right)$$

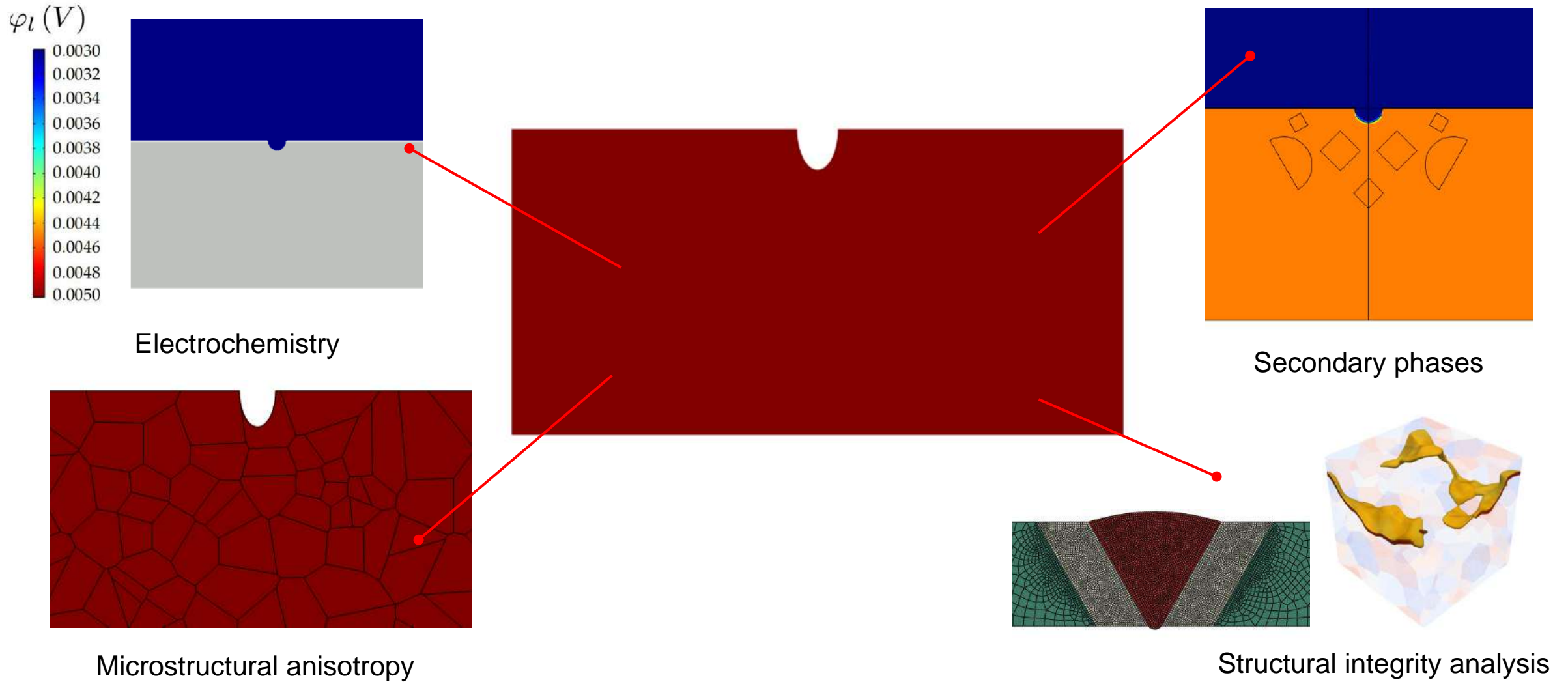
$$\frac{\partial c}{\partial t} - \nabla \cdot D \nabla [c - h(\phi)(c_{Se} - c_{Le}) - c_{Le}] = 0$$

A new phase field paradigm: corrosion

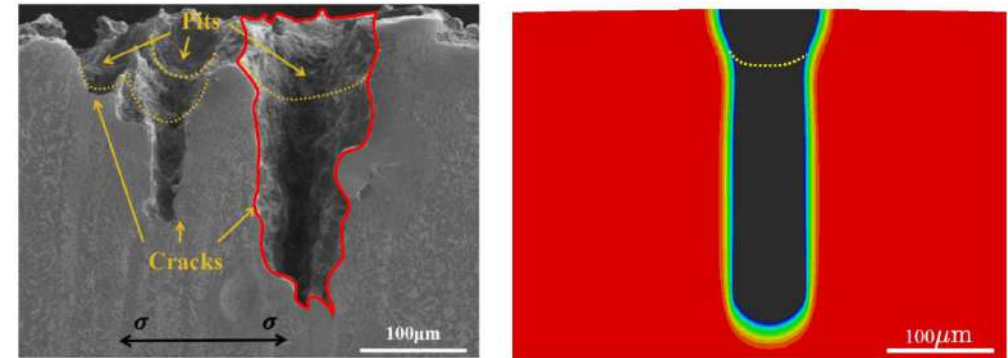
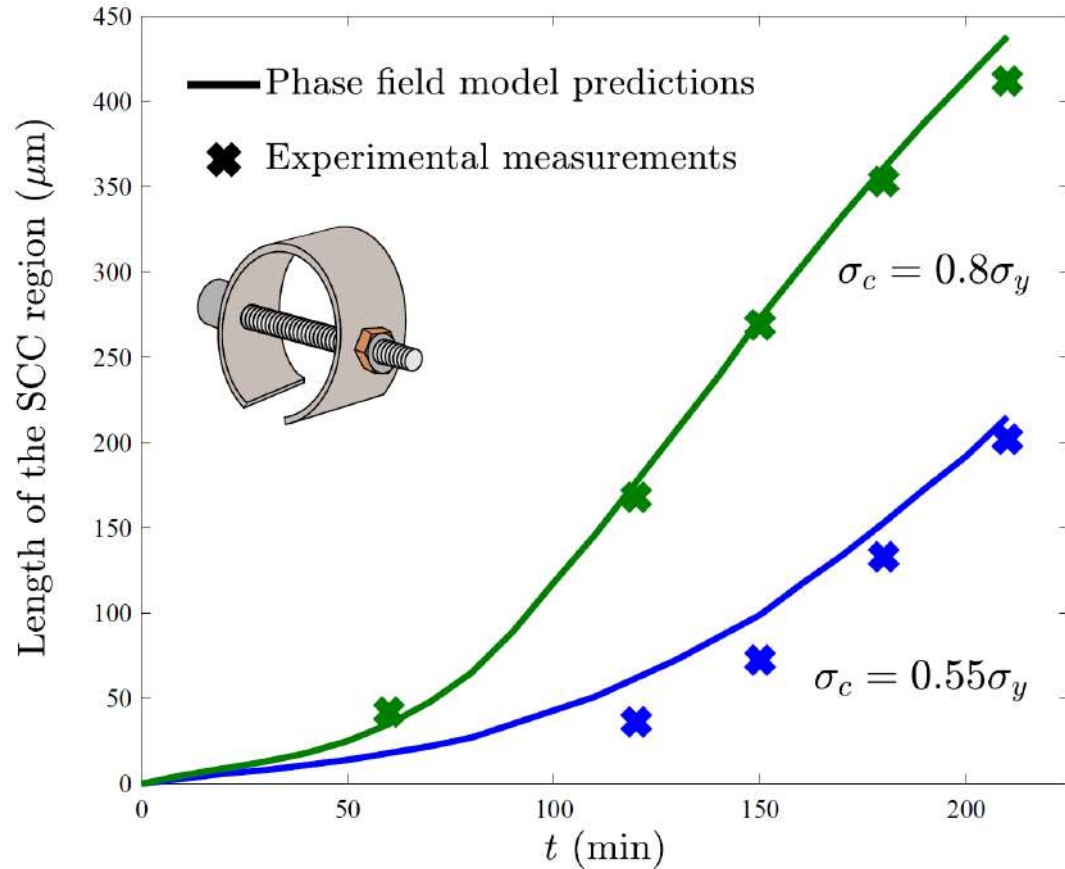


Cui, Ma, Martínez-Pañeda. *JMPS* (2021)

A new phase field paradigm: corrosion



Representative result: C-ring test



- The model quantitatively captures the sensitivity of corrosion kinetics to applied mechanical load

Cui, Ma, Martínez-Pañeda. *JMPS* (2021)

Environmentally
assisted cracking

☐ Stress Corrosion
Cracking (SCC)

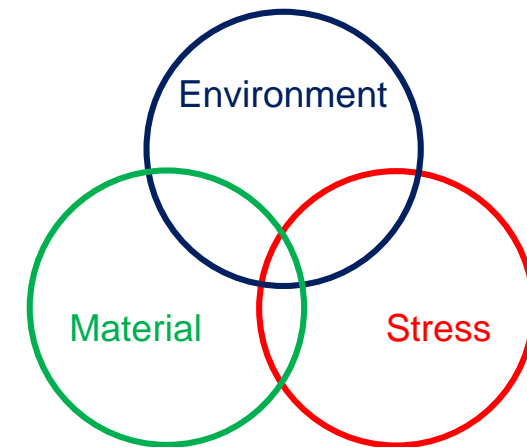
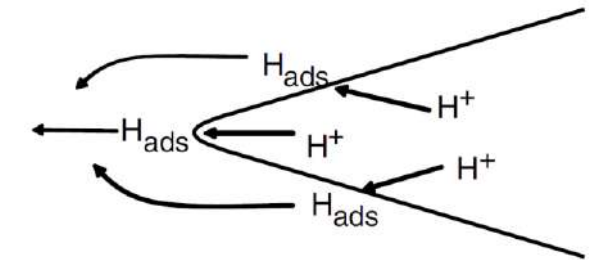
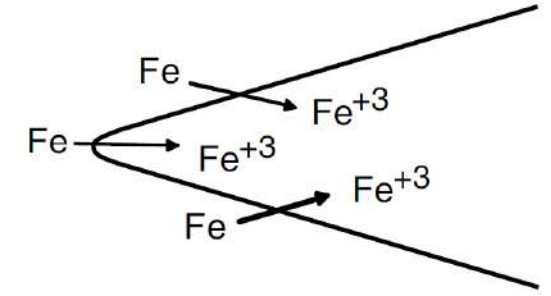
☐ Anodic-dissolution
cracking

☐ Hydrogen embrittlement

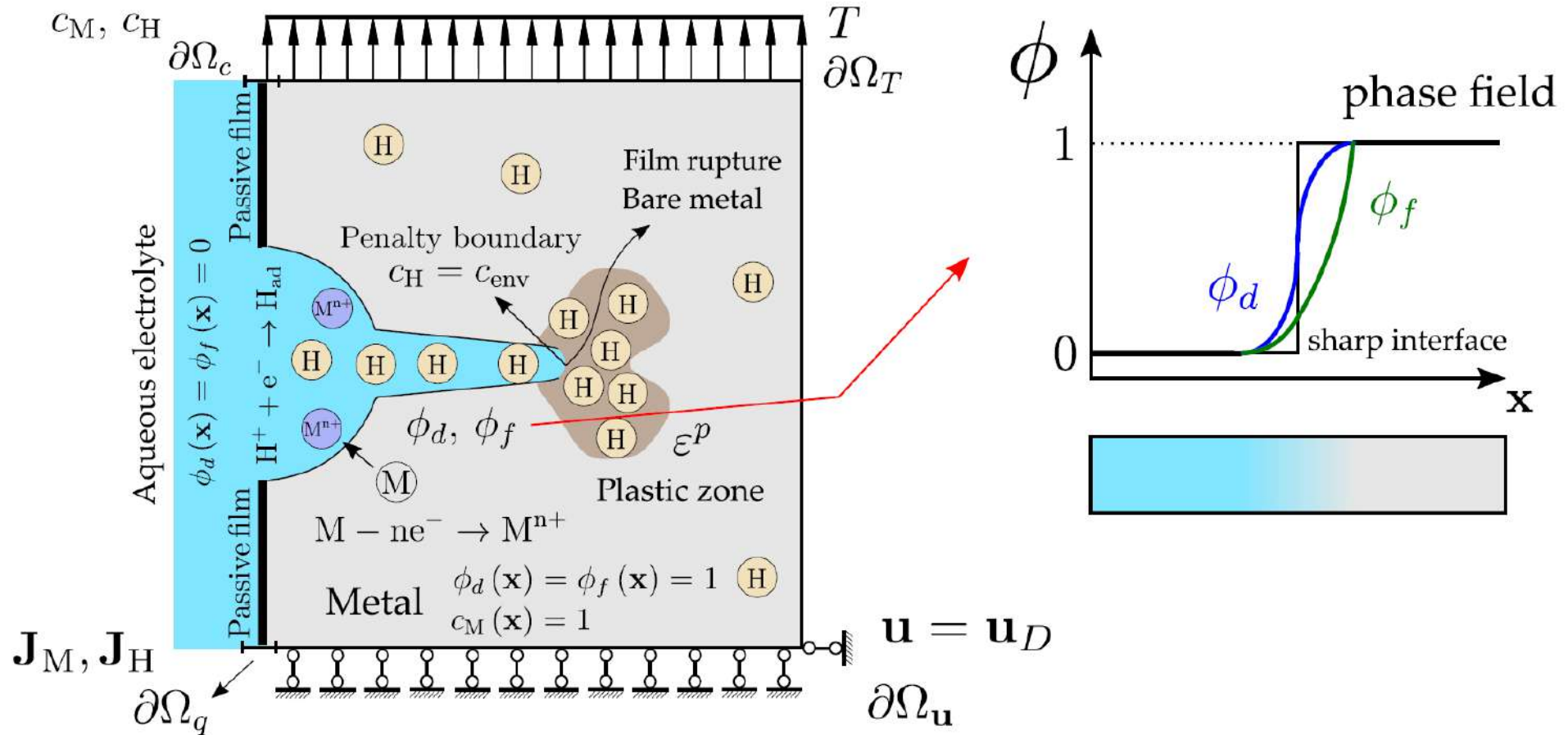
☐ Hydrogen embrittlement

☐ Liquid Metal Embrittlement

☐ Oxidation fatigue, *etc.*



A generalised model for SCC



Cui, Ma, Martínez-Pañeda (JMPS, 2022)

A generalised model for SCC

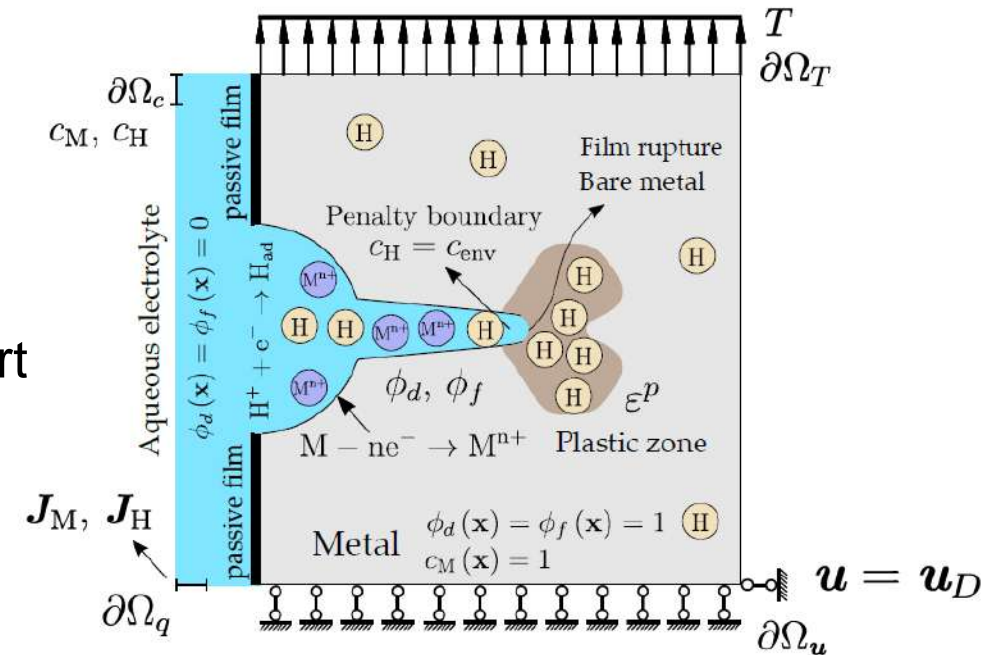
$$\nabla \cdot [h_d(\phi_d)h_f(\phi_f)\boldsymbol{\sigma}] = \mathbf{0} \quad \text{Displacement}$$

$$h'_f(\phi_f) h_d(\phi_d) \psi_0^m - G_c(c_H) \left(\frac{1 - \phi_f}{\ell_f} + \ell_f \nabla^2 \phi_f \right) = 0 \quad \text{Fracture}$$

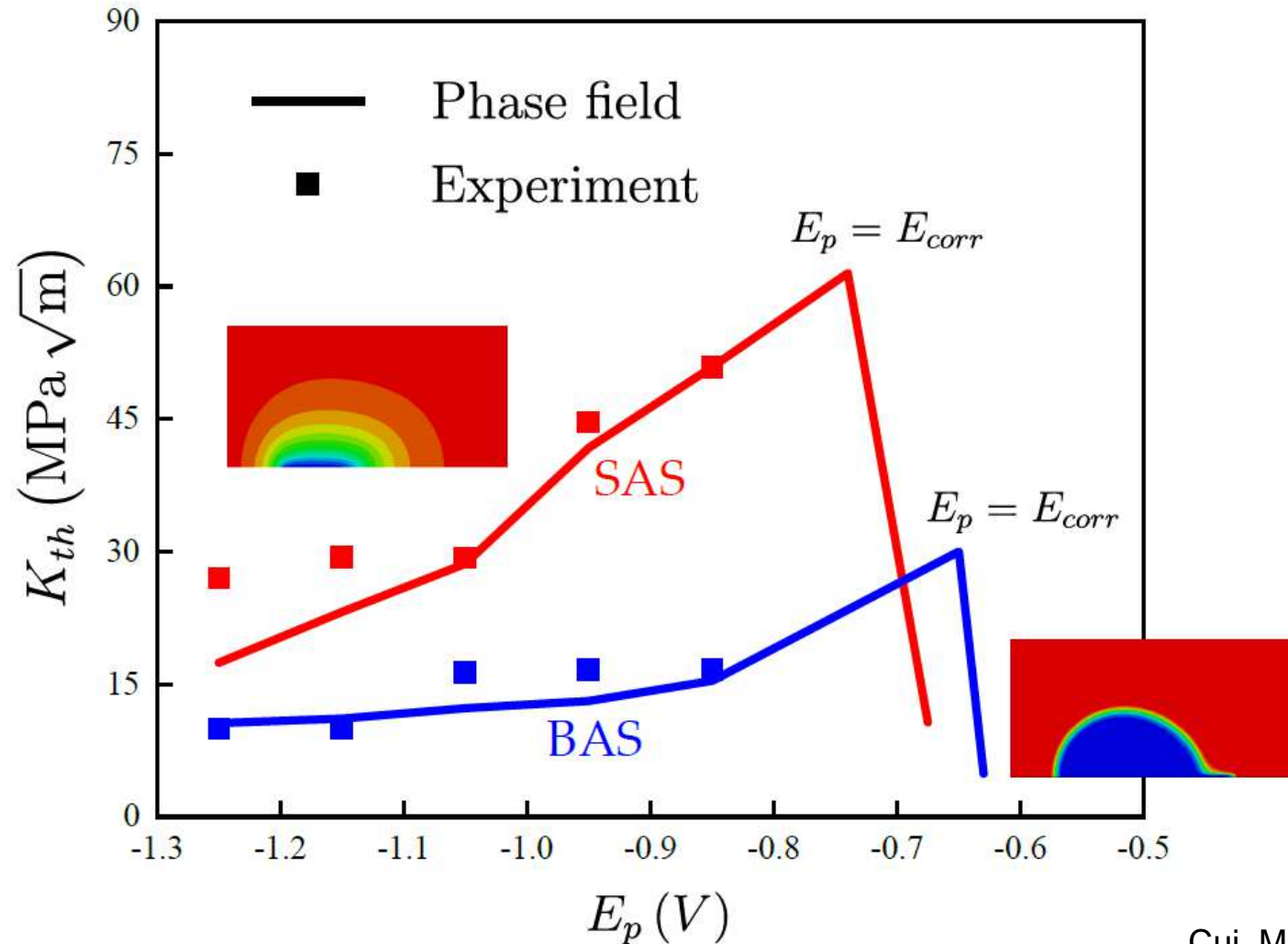
$$\frac{dc_H}{dt} - D_H \nabla c_H + \frac{D_H c_H}{RT} \bar{V}_H \nabla \sigma_h = 0 \quad \text{H diffusion}$$

$$\frac{dc_M}{dt} - \nabla \cdot D_M \nabla [(c_M - h_d(\phi_d)(c_{Se} - c_{Le}) - c_{Le})] = 0 \quad \text{Ionic transport}$$

$$\frac{d\phi_d}{dt} + L(\varepsilon^p, \sigma_h) \left(\frac{\partial \psi^{ch}}{\partial \phi_d} - \alpha \nabla^2 \phi_d \right) = 0 \quad \text{Corrosion}$$



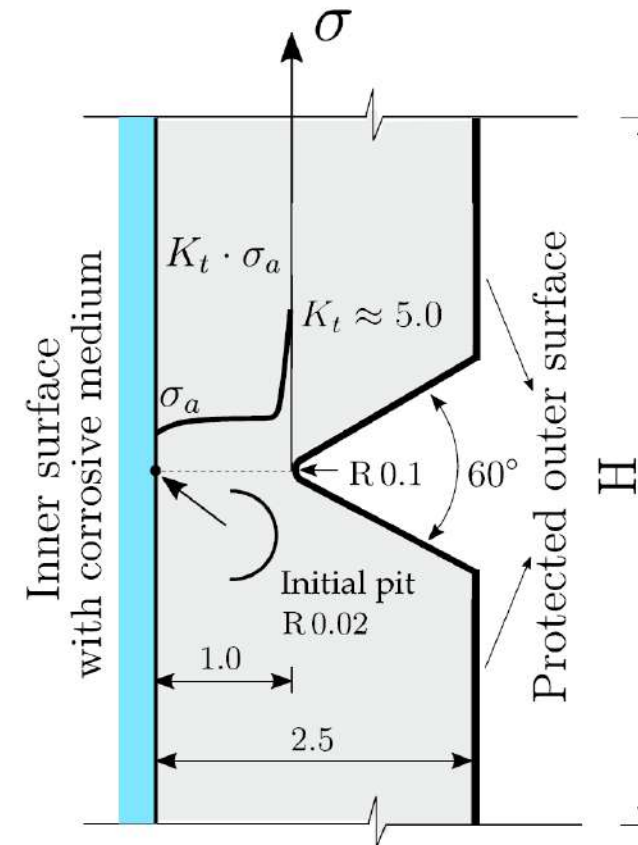
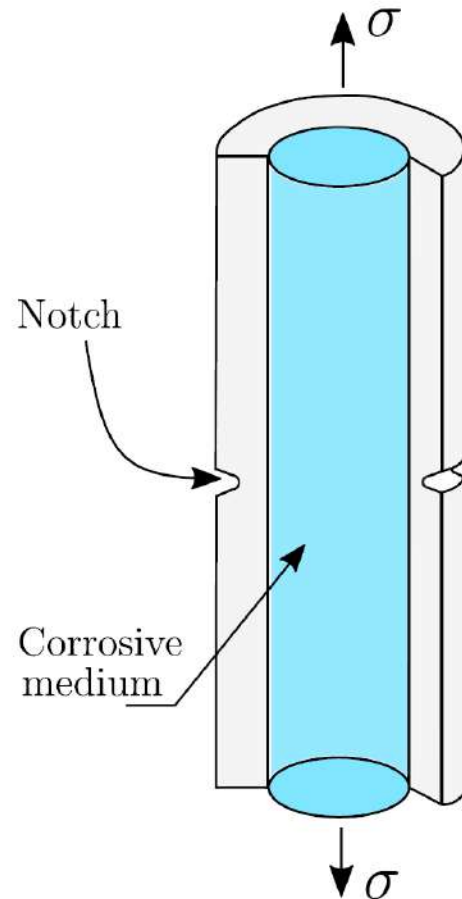
Cui, Ma, Martínez-Pañeda (JMPS, 2022)



Cui, Ma, Martínez-Pañeda (JMPS, 2022)

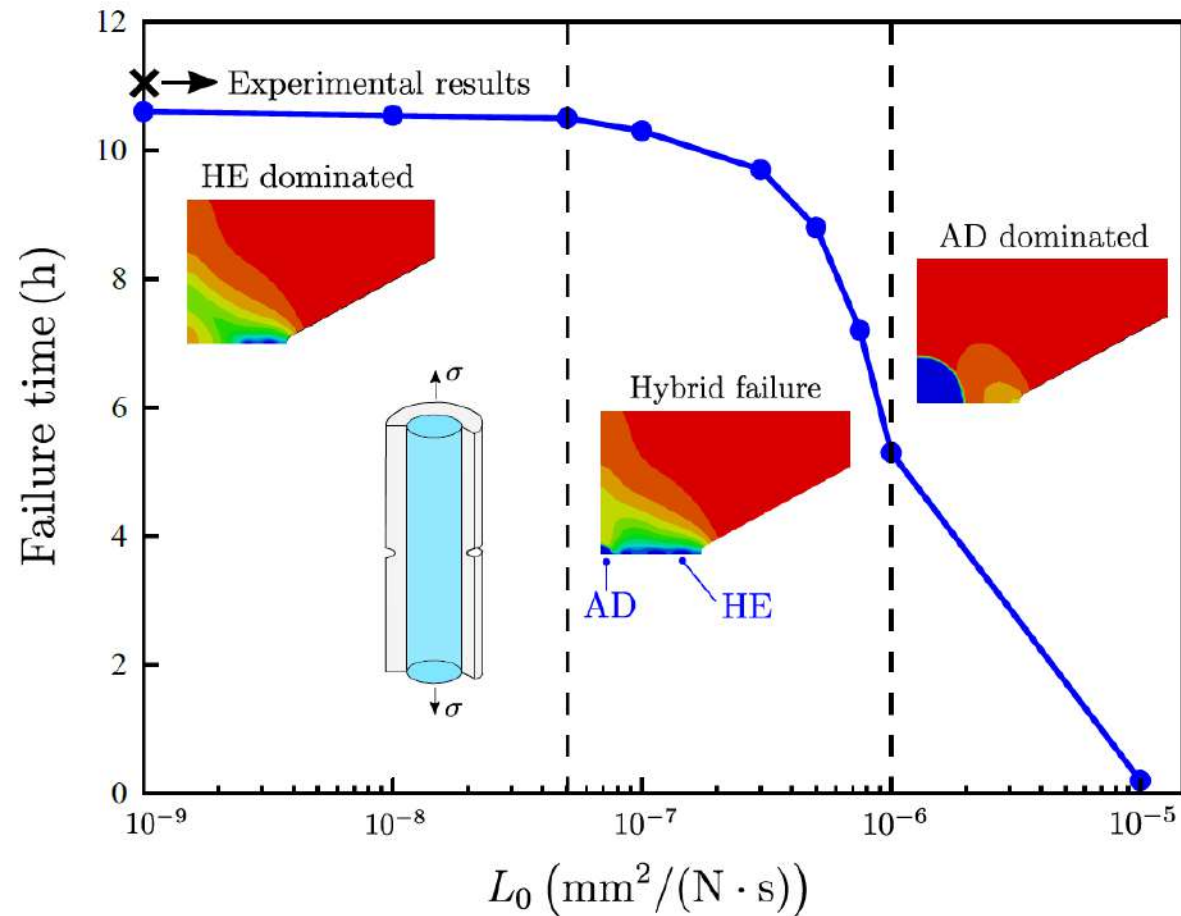
A generalised model for SCC

Gruhl (1984) experiments in Al alloys



Cui, Ma, Martínez-Pañeda (JMPS, 2022)

Gruhl (1984) experiments in Al alloys



Cui, Ma, Martínez-Pañeda (JMPS, 2022)

Concluding remarks

- Phase field and multi-physics modelling can be combined to develop a mechanistic computational framework that resolves the physics processes of hydrogen embrittlement

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- The framework is general, can accommodate any mechanistic interpretation of H embrittlement and can readily be extended (microstructure, welds, stress corrosion cracking, *etc.*)

Concluding remarks

- Phase field and multi-physics modelling can be combined to develop a mechanistic computational framework that resolves the physics processes of hydrogen embrittlement
- The computational framework developed can predict fracture (and fatigue) in laboratory tests and practical applications (*Virtual Testing*)
- The framework is general, can accommodate any mechanistic interpretation of H embrittlement and can readily be extended (microstructure, welds, stress corrosion cracking, *etc.*)
- The combination of phase field and multi-physics modelling enables developing computational models that can resolve the physical processes of corrosion damage

Thank you

- Codes are openly shared! www.imperial.ac.uk/mechanics-materials



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